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Re: West End<br>2022 Update<br>Eagle County, CO<br>LSC \#220510

Dear Mr. Murphy:
In response to your request, LSC Transportation Consultants, Inc. has prepared this updated traffic impact analysis for the proposed West End development (the site) and the adjacent Gashouse and Edwards Plaza parcels (the impact area) to address preliminary feedback from CDOT. As shown on Figure 1, the site is located north of US Highway 6 and west of the Edwards Access Road in the Edwards community of Eagle County, Colorado.

## REPORT CONTENTS

The report contains the following: the existing roadway and traffic conditions in the vicinity of the site including the lane geometries, traffic controls, posted speed limits, etc.; the existing weekday peak-hour traffic volumes; the typical weekday site-generated traffic volume projections for the site and impact area; the assignment of the projected traffic volumes to the area roadways; the projected long-term background and resulting total traffic volumes on the area roadways; the site's and impact area's projected traffic impacts; and any recommended roadway improvements to mitigate the site's and impact area's traffic impacts or the impacts from growth in background traffic. All work is consistent with the approved TIS methodology form which is attached for reference.

## LAND USE AND ACCESS

## New West End PUD

The new West End PUD land use proposal consists of approximately 275 multi-family workforce dwelling units (see Figure 2).

## Loop Road

The new West End PUD will be served by a "loop road" around an enlarged Gashouse parcel (Loop Road) as shown in Figure 2. The proposed Loop Road involves a land exchange between
the West End, Gashouse and Edwards Plaza owners. The Gashouse parcel's existing US Highway 6 access point would be relocated to the west to accommodate the additional land for the Gashouse parcel and become the southern end of the Loop Road (Intersection \#3). The Gashouse parcel would be accessed from a new access to the Loop Road, with no US Highway 6 or Edwards Access Road direct access. The eastern end of the Loop Road would terminate at Edwards Access Road (Intersection \#4).

The Loop Road in conjunction with the recently constructed roundabout at US Highway 6 and Edwards Access Road facilitates full mobility ingress and egress from all directions using only right-in and right-out turn movements.

## Site Access to Loop Road

The site will access the Loop Road as shown in Figure 2. There will be separate ingress and egress locations to allow for easy turn around with no backing maneuver. There will be minimal queuing on the Loop Road considering both ends are right-in/right-out movement. The ingress location is located a sufficient distance from US Highway 6 so no queuing issues are expected.

## Impact Area/Northwest Corner of Edwards

## Edwards Plaza

The existing uses of the Edwards Plaza parcels, which are traffic-intense commercial uses, are assumed to remain for purposes of this traffic impact study.

## Gashouse Parcel

The owner of the Gashouse property has not indicated any near-term redevelopment plans. For the purpose of this traffic impact study, a high trip generation potential of 3,000 square feet restaurant with drive-through use was assumed.

## AREA ROADWAYS

## Major Roadways

The major roadways in the vicinity of the site and impact area are shown on Figure 1 and are described below.

- US Highway 6 is an east-west, two-lane US Highway south of the site. It is designated by CDOT as Non-Rural Principal Highway (NR-A) per the attached CDOT Straight Line Diagram. The intersection with Edwards Access Road is controlled by a recently constructed modern two-lane roundabout (the "2019 Edwards Roundabout"). The posted speed limit in the vicinity of the site is 35 mph east of Edwards Access Road and 45 mph west of Edwards Access Road. US 6 is planned to be widened to four lanes adjacent to the site by 2040.
- Edward Access Road is a north-south, four-lane principal arterial roadway east of the site. The intersection with US Highway 6 is roundabout-controlled. The posted speed limit in the vicinity of the site is 35 mph .


## BACKGROUND INFORMATION

## 2019 Edwards Roundabout

The Edwards River Park (ERP) proposed development is located on the former quarry site north of the intersection of US Highway 6 and Lake Creek Road. In connection with the proposed ERP development, the April 4, 2019 ERP traffic impact study was conducted by McDowell Engineering (ERP TIS). Final plans had been prepared and construction was about to begin on the 2019 Edwards Roundabout when CDOT and Eagle County expressed concerns that the ERP TIS indicated higher traffic volume projections than the previous design traffic volumes for the 2019 Edwards Roundabout. These concerns were addressed in a memo from Felsburg, Holt \& Ullevig dated May 15, 2019 (FHU Memo). The new higher traffic volume forecast from the FHU Memo were referred to MSA Professional Services, Inc. and MSA/Ourston was tasked with updating the operational analysis of the 2019 Edwards Roundabout.

Taking into consideration the new higher traffic volume forecasts, a MSA memo dated May 23, 2019 (2019 MSA/Ourston Memo) concluded that although the 2019 Edwards Roundabout is not a complete solution to the traffic concerns of Edwards, the 2019 Edwards Roundabout is the best available alternative:
"For validation of the decision to construct a roundabout at this intersection, consideration should be given to the operation of a traffic signal alternative with a similar lane configuration and property impacts. If a traffic signal operates with similar, or more, congestion than the roundabout near the Design Year (2019), the roundabout alternative is still the more prudent intersection improvement based on safety benefits. A roundabout will operate better for all approaches during the off-peak periods and any potential crashes at the intersection will be less severe with a roundabout in place."

## FHU Memo Projected Traffic vs. Currently Projected Traffic

The FHU Memo assumed 200 multi-family units and 100,000 square feet of commercial space for the combined West End and Vogelman parcels, which were assumed to have a weekday daily trip generation potential of 5,600 trips. In comparison, the new West End PUD proposes only 275 multi-family units, which is estimated to have a weekday daily trip generation potential considerably below the FHU Memo assumptions.

The FHU Memo did not assume any future development for the Gashouse parcel. However, even when assuming the most traffic-intense future use of the potential future land use options for the Gashouse parcel, the predicted traffic for the combined West End, Vogelman and Gashouse parcels still result in a net reduction of about 640 daily trips relative to what was previously assumed in the FHU Memo for only the West End and Vogelman parcels (i.e., nothing assumed for the Gashouse parcel).

## 2019 Edwards Roundabout/No West End Development

Out of an abundance of caution and to alleviate any risk that future traffic issues of the 2019 Edwards Roundabout are inaccurately attributed to the anticipated development of the West End parcel and impact area parcels, please see the comparisons of background traffic and total
traffic level of service rates in Table 1. The poor levels of service in the study area are expected to occur with or without the proposed developments.

## TRAFFIC CONDITIONS

## Existing Traffic Conditions

Figure 3a shows the existing early March, 2020 traffic volumes in the vicinity of the site and impact area on a typical weekday and Figure 3b shows the seasonally adjusted traffic volumes based on a seasonal factor of 1.14 from March to September. The seasonal adjustment factor spreadsheet is attached for reference. The weekday peak-hour traffic volumes in Figure 3a are from the attached traffic counts conducted by Counter Measures on March $3^{\text {rd }}$ and $4^{\text {th }}, 2020$. Figure 3c shows the existing lane geometries, traffic controls, and posted speed limits.

## 2025 and 2040 Background Traffic

Figure 4a shows the estimated 2025 background traffic based on an annual growth rate of onehalf percent plus buildout of the Edwards River Park (ERP) project per the approved TIS methodology form. Figure 4b shows the 2025 lane geometry and traffic control.

Figure 5a shows the trips estimated for the West End and Vogelman parcels in the April 4, 2019 ERP Traffic Study (ERP TIS) by McDowell Engineering - excerpts from this study are attached for reference. Per the approved TIS methodology form, these volumes were subtracted from the 2040 total traffic volumes provided by CDOT in the May 15, 2019 FHU Memorandum (FHU Memo) which is attached for reference. Figure 5b shows the 2040 background traffic and Figure 5c shows the 2040 background lane geometry and traffic control.

## Existing, 2025, and 2040 Background Levels of Service

Level of service (LOS) is a quantitative measure of the level of congestion or delay at an intersection. Level of service is indicated on a scale from "A" to "F." LOS A is indicative of little congestion or delay and LOS F is indicative of a high level of congestion or delay. Attached are specific level of service definitions for unsignalized intersections.

The intersections in Figures 3b through 5c were analyzed as appropriate to determine the existing, 2025 background, and 2040 background levels of service using Synchro and Rodel. Table 1 shows the level of service analysis results. The level of service reports are attached.

1. US 6/Edwards Access Road: This roundabout-controlled intersection currently operates at an overall LOS "A" during both morning and afternoon peak-hours and is expected to operate at LOS "B" or better through 2025 and LOS "C" by 2040. There are individual approaches expected to operate at LOS "E" or "F" by 2040.
2. US 6/Edwards Village Center Access: All movements at this stop-sign controlled intersection currently operate at LOS "C" or better during both morning and afternoon peakhours and are expected to do so through 2040 with the following exception: The northbound approach operates at LOS " $F$ " during the afternoon peak-hour and is expected to do so through 2040. The intersection may eventually need to be converted to three-quarter movement.
3. US 6/Gashouse Access (Proposed Loop Road): This intersection was only evaluated in the total traffic scenarios.
4. Edwards Access Road/Edwards Plaza Secondary Access (Proposed Loop Road)/Riverwalk Access RIRO): All movements at this stop-sign controlled intersection currently operate at LOS "B" or better during both morning and afternoon peak-hours and are expected to do so through 2040 with the following exception: The westbound right-turn movement (i.e., trips exiting Riverwalk) operates at LOS " F " in the afternoon peak-hour and is expected to do so through 2040 primarily due to the heavy volume of turning traffic.
5. Edwards Access Road/Edwards Plaza Primary Access (Three-Quarter): All movements at this stop-sign controlled intersection currently operate at LOS "B" or better during both morning and afternoon peak-hours and are expected to operate at LOS "C" or better through 2040.

## TRIP GENERATION

Table 2 shows the estimated average weekday, morning peak-hour, and afternoon peak-hour trip generation for the proposed site based on the rates from Trip Generation, $11^{\text {th }}$ Edition, 2021 by the Institute of Transportation Engineers (ITE).

The site is projected to generate about 1,837 vehicle-trips on the average weekday, with about half entering and half exiting during a 24 -hour period. During the morning peak-hour, which generally occurs for one hour sometime between 6:30 and 8:30 a.m., about 26 vehicles would enter and about 82 vehicles would exit the site. During the afternoon peak-hour, which generally occurs for one hour sometime between 4:00 and 6:00 p.m., about 75 vehicles would enter and about 75 vehicles would exit.

The Gashouse parcel is projected to generate about 1,402 vehicle-trips on the average weekday, with about half entering and half exiting during a 24 -hour period. During the morning peakhour, which generally occurs for one hour sometime between 6:30 and 8:30 a.m., about 68 vehicles would enter and about 66 vehicles would exit the site. During the afternoon peak-hour, which generally occurs for one hour sometime between 4:00 and 6:00 p.m., about 52 vehicles would enter and about 48 vehicles would exit.

These estimates assume 43 percent passby trips for the Gashouse Parcel restaurant use consistent with the ITE Trip Generation Handbook, $3^{\text {rd }}$ Edition. No internal trips or alternative travel mode trips were assumed to maintain a conservative analysis.

## TRIP DISTRIBUTION

Figure 6 shows the estimated directional distribution of the site-generated and impact area generated traffic volumes on the area roadways. The estimates were based on the location of the two parcels with respect to the regional population, employment, and activity centers; and the site's proposed land use. These assumptions are consistent with the approved TIS methodology form.

## TRIP ASSIGNMENT

Figure 7a shows the estimated West End Parcel site-generated traffic volumes based on the West End trip generation estimate (from Table 2) and the residential directional distribution in Figure 6.

Figure 7 b shows the estimated Gashouse Parcel primary site-generated traffic volumes based on the Gashouse primary trip generation estimate (from Table 2) and the commercial directional distribution in Figure 6.

Figure 7c shows the estimated Gashouse Parcel passby site-generated traffic volumes based on the Gashouse pass-by trip generation estimate (from Table 2).

Figure 7 d is the assignment of total site-generated and impact area generated trips and is the sum of the traffic volumes in Figures 7a through 7c.

## 2025 AND 2040 TOTAL TRAFFIC

Figure 8a shows the 2025 total traffic which is the sum of 2025 background traffic volumes (from Figure 4 a ) and the total site-generated traffic volumes (from Figure 7d) Figure 8b shows the recommended lane geometry and traffic control.

Figure 9a shows the 2040 total traffic which is the sum of 2040 background traffic volumes (from Figure 5b) and the total site-generated traffic volumes (from Figure 7d). Figure 9b shows the 2040 recommended lane geometry and traffic control. Figure 9a also shows the 2040 roundabout peak-hour traffic volumes provided by CDOT in the FHU Memo.

## PROJECTED LEVELS OF SERVICE

The intersections in Figures 8a through 9b were analyzed to determine the 2025 and 2040 total traffic levels of service. Table 1 shows the level of service analysis results. The level of service reports are attached.

1. US 6/Edwards Access Road: This roundabout-controlled intersection is expected to operate at an overall LOS "A" during the morning peak-hour and LOS "C" during the afternoon peak-hour through 2025. In 2040, the morning peak-hour is expected to operate at LOS "E" and the afternoon peak-hour is expected to operate at LOS "D". There are individual approaches expected to operate at LOS " F " in both peak-hours. The same analysis was run for 2040 total traffic using the traffic volumes provided by CDOT in the May 15, 2019 FHU Memorandum which resulted in slightly better operations in the morning peakhour improving from 43.7 seconds (LOS "E") to 36.8 seconds (LOS "E") but considerably worse operations in the afternoon peak-hour degrading from 29.8 seconds (LOS "D") to 73.3 seconds (LOS " F "). This is primarily due to the currently proposed land uses having a considerably lower trip generation potential in the afternoon peak-hour than assumed in the FHU Memo.
2. US 6/Edwards Village Center Access/West End Access: All movements at this stop-sign controlled intersection are expected to operate at LOS "D" or better during both morning
and afternoon peak-hours through 2040 with the exception of the northbound approach. The intersection may need to be converted to three-quarter movement by 2040.
3. US 6/Gashouse Access (Proposed Loop Road) (RIRO): All movements at this stop-sign controlled intersection are expected to operate at LOS "C" or better during both morning and afternoon peak-hours through 2040.
4. Edwards Access Road/Edwards Plaza Secondary Access (Proposed Loop Road)/Riverwalk Access (RIRO): All movements at this stop-sign controlled intersection are expected to operate at LOS "C" or better during both morning and afternoon peak-hours through 2040 with the following exception: The westbound right-turn movement (i.e., trips exiting Riverwalk) is expected to operate at LOS " F " in the afternoon peak-hour through 2040 primarily due to the heavy volume of turning traffic.
5. Edwards Access Road/Edwards Plaza Primary Access (Three-Quarter): All movements at this stop-sign controlled intersection are expected to operate at LOS "C" or better during both morning and afternoon peak-hours through 2040.

## RIGHT-TURN AUXILIARY LANE ANALYSIS AT THE THREE SITE ACCESS INTERSECTIONS

Based on feedback from CDOT, Intersections \#3 and \#4 were revisited to determine if right-turn deceleration and acceleration lanes are needed for the right-turn movements in and out of the site. Intersections \#3 and \#4 are proposed as right-in/right-out site access points.

## Intersection \#3:

Deceleration Lane - Figure 9a shows the right-turn movement into the site is expected to peak at about 84 vehicles per hour in the afternoon peak hour by 2040. US 6 in this location has a 45 mph posted speed limit but the intersection is located only about 250 feet downstream from the existing roundabout so approaching westbound travel speeds are expected to be below 45 mph . A westbound to northbound right-turn deceleration lane would typically be required on US 6 approaching this intersection based on the posted speed limit and projected turning volume. The typical length required would be a 273 -foot long lane plus a 162 -foot transition taper. The distance between Intersection \#3 and the existing roundabout is only about 250 feet so any right-turn lane would need to be substandard in length. A review of the properties in this location suggest a 60-foot right-turn lane plus a 75 -foot transition taper would likely fit in the space available. The vehicle speeds exiting the existing roundabout should be in the range of $25-30 \mathrm{mph}$ so a substandard lane would likely provide a benefit if desired by CDOT.

Acceleration Lane - Figure 9a shows the right-turn movement out of the site is expected to peak at about 39 vehicles per hour in the morning peak hour by 2040 - this volume is well below 50 vehicles per hour and is expected to operate at acceptable levels of service so no acceleration lane is required.

## Intersection \#4:

Deceleration Lane - Figure 9a shows the right-turn movement into the site is expected to peak at about 48 vehicles per hour in the afternoon peak hour by 2040. Edwards Access Road in this location has a 35 mph posted speed limit. A southbound to westbound right-turn deceleration
lane would typically be required on Edwards Access Road approaching this intersection based on the posted speed limit and projected turning volume. The typical length required would be a 190 -foot long lane plus a 120 -foot transition taper. There are three reasons why this lane is not recommended. First, the construction of this lane would materially impact the adjacent property, Edwards Plaza, by requiring all of its existing parking spaces on the eastern side of Edwards Plaza I to be eliminated to accommodate the deceleration lane. Recall, the proposed Loop Road requires the participation of Edwards Plaza and the Gashouse in a land exchange with the West End. The project team feels that a deceleration lane at this location, and the associated loss of parking spaces on the eastern side of Edwards Plaza I, would be fatal to obtaining Edwards Plaza's required consent because these parking spaces serve retail along the eastern side of Edwards Plaza I ${ }^{1}$. Second, the outside southbound lane on Edwards Access Road is a right-turn-only lane at the existing roundabout so traffic approaching the roundabout will already be decelerating given the close proximity of this intersection to the roundabout (approximately 150 feet). Third, the southbound movement at the roundabout is expected to have queuing at peak times in future years that may periodically back up through Intersection \#4. The project team's concern is providing a southbound deceleration lane would allow southbound vehicles to exit the southbound Edwards Access Road queue a few hundred feet further north making the Loop Road attractive as a roundabout bypass during peak traffic conditions. The project team feels not providing this deceleration lane would make the Loop Road much less attractive as a roundabout bypass.

Acceleration Lane - Figure 9a shows the right-turn movement out of the site is expected to peak at about 119 vehicles per hour in the morning peak hour by 2040. The posted speed limit is below 45 mph and the movement is expected to operate at acceptable levels of service so no acceleration lane is required.

## CONCLUSIONS AND RECOMMENDATIONS

## Trip Generation

1. The site is projected to generate about 1,837 vehicle-trips on the average weekday, with about half entering and half exiting during a 24 -hour period. During the morning peakhour, which generally occurs for one hour sometime between 6:30 and 8:30 a.m., about 26 vehicles would enter and about 82 vehicles would exit the site. During the afternoon peak-hour, which generally occurs for one hour sometime between 4:00 and 6:00 p.m., about 75 vehicles would enter and about 75 vehicles would exit.
2. The Gashouse parcel is projected to generate about 1,402 vehicle-trips on the average weekday, with about half entering and half exiting during a 24 -hour period. During the morning peak-hour, which generally occurs for one hour sometime between 6:30 and 8:30 a.m., about 68 vehicles would enter and about 66 vehicles would exit the site. During the afternoon peak-hour, which generally occurs for one hour sometime between 4:00 and 6:00 p.m., about 52 vehicles would enter and about 48 vehicles would exit. These estimates assume 43 percent passby trips for the Gashouse Parcel restaurant use consistent with the ITE Trip Generation Handbook, $3^{\text {rd }}$ Edition. No internal trips or alternative travel mode trips were assumed to maintain a conservative analysis.
[^0]
## Projected Levels of Service

3. The roundabout controlled US 6/Edwards Road intersection (i.e., 2019 Edwards Roundabout) is expected to operate at an overall LOS "E" during the morning peak-hour and LOS "D" during the afternoon peak-hours in 2040 with individual approaches operating at LOS "F". The prior land uses assumed in the ERP TIS and the FHU Memo would also operate at LOS "E" in the morning peak-hour but degrade from LOS "D" to LOS "F" in the afternoon peak-hour. This is primarily due to the prior land uses having a much higher trip generation potential in the afternoon peak-hour than for the currently proposed land uses.
4. All movements at the stop-sign controlled intersections (i.e., Intersections \#2, \#3, \#4, and \#5) are expected to operate at LOS "D" or better through 2040 with the following exceptions: The northbound approach at the US 6/Edwards Village Center/ West End intersection is expected to operate at LOS " F " during both peak-hours. The intersection may need to be converted to three-quarter movement by 2040. The westbound right-turn movement (i.e., trips exiting Riverwalk) at the Edwards Access Road/Edwards Plaza Secondary Access (Proposed Loop Road)/Riverwalk (RIRO) is expected to operate at LOS "F" in the afternoon peak-hour primarily due to the heavy volume of turning traffic. This LOS "F" does not materially affect the function of the Proposed Loop Road as it is separated from it across the Edwards Access Road by a raised center median.

## Recommendations

5. The West End site proposes residential use only. Eliminating commercial uses helps to reduce the previously identified impacts to the surrounding roadway network.
6. A right-turn lane may be appropriate at Intersection \#3 based on CDOT's review of this analysis. No acceleration lanes are recommended at the site access intersections (Intersections \#3 and \#4). We are available to discuss at length as the project moves through the review process. Figure 10 shows additional conceptual detail for the site access and loop road including a proposed bus stop relocation.
7. The Loop Road and general internal site connectivity shown in Figures 2 and 10 should be implemented to maximize the benefits of the adjacent roundabout.

We trust our findings will assist you in gaining approval of the proposed West End PUD. Please contact me if you have any questions or need further assistance.

Sincerely,
LSC TRANSPORTATION CONSUTTANTS, INC.

By


Principal
CSM/wc

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6-27-22
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Enclosures: Tables 1 and 2
Figures 1-10
TIS Methodology Form
CDOT Straight Line Diagram
Seasonal Adjustment Spreadsheet
Traffic Count Reports
Excerpts from April 4, 2019 ERP TIS by McDowell Engineering (ERP TIS)
FHU Memorandum dated May 15, 2019 (FHU Memo)
Level of Service Definitions
Level of Service Reports
W: \LSC $\backslash$ Projects $\backslash 2022 \backslash 220510-W e s t E n d-2022$ Update $\backslash$ Report $\backslash$ WestEnd-062722.wpd

| Intersection Location | Traffic Control | Table 1 <br> Intersection Levels of Service Analysis <br> West End - 2022 Update Eagle County, CO <br> LSC \#220510; June, 2022 |  |  |  |  |  | $2040$ <br> Background Traffic |  | $\begin{gathered} 2040 \\ \text { Total Traffic } \end{gathered}$ |  | 2040 Total Traffic CDOT - FHU ${ }^{(1)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Existing Traffic |  | $2025$ <br> Background Traffic |  | $\begin{gathered} 2025 \\ \text { Total Traffic } \end{gathered}$ |  |  |  |  |  |  |  |
|  |  | Level of Service AM | Level of Service PM | Level of Service AM | $\begin{gathered} \hline \text { Level of } \\ \text { Service } \\ \text { PM } \\ \hline \hline \end{gathered}$ | Level of Service AM | Level of Service PM | Level of Service AM | Level of Service PM | Level of Service AM | Level of Service PM | Level of Service AM | Level of Service PM |
| 1) US 6/Edwards Access Road | Roundabout |  |  |  |  |  |  |  |  |  |  |  |  |
| EB Approach |  | A | A | A | B | A | B | A | F | A | F | A | F |
| WB Approach |  | A | B | A | C | A | D | E | A | F | B | F | B |
| NB Approach |  | A | A | A | B | A | C | D | A | D | B | D | B |
| SB Approach |  | A | A | A | A | A | B | A | B | A | B | A | B |
| Entire Intersection Delay (sec/veh) |  | 5.7 | 7.8 | 6.5 | 14.2 | 7.3 | 19.5 | 24.2 | 22.9 | 43.7 | 29.8 | 36.8 | 73.3 |
| Entire Intersection LOS |  | A | A | A | B | A | C | C | C | E | D | E | F |
| 2) US 6/Edwards Village Center Access | TWSC |  |  |  |  |  |  |  |  |  |  |  |  |
| NB Approach |  | C | F | C | F | D | F | F | F | F | F |  |  |
| WB Left |  | A | B | B | B | B | B | B | B | B | B |  |  |
| Entire Intersection LOS |  | 16.8 | >240 | 24.8 | >240 | 28.4 | >240 | 52.8 | 114.8 | 54.0 | 125.6 |  |  |
| 3) US 6/Gashouse Access (Proposed Loop Road) | TWSC |  |  |  |  |  |  |  |  |  |  |  |  |
| SB Approach | RIRO | -- | -- | -- | -- | B | B | -- | -- | B | C |  |  |
| Critical Movement Delay(sec /veh) |  | -- | -- | -- | -- | 10.8 | 13.8 | -- | -- | 12.1 | 16.1 |  |  |
| 4) Edwards Access Road/Edwards Plaza Secondary | TWSC |  |  |  |  |  |  |  |  |  |  |  |  |
| Access (Proposed Loop Road/Riverwak Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| EB Right | RIRO | B | B | B | B | B | B | B | B | C | C |  |  |
| WB Right |  | B | F | B | F | B | F | C | F | C | F |  |  |
| Critical Movement Delay(sec /veh) |  | 12.0 | 75.9 | 12.7 | 132.9 | 13.0 | 144.1 | 15.6 | 96.1 | 16.0 | 104.5 |  |  |
| 5) Edwards Access Road/Edwards Plaza | TWSC |  |  |  |  |  |  |  |  |  |  |  |  |
| Primary Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| NB Left | Three- | A | A | A | B | A | B | B | B | B | B |  |  |
| EB Right | Quarter | B | B | B | B | B | B | B | C | B | C |  |  |
| Critical Movement Delay(sec/veh) |  | 10.6 | 12.1 | 11.2 | 14.5 | 11.3 | 14.9 | 12.6 | 18.5 | 12.7 | 19.2 |  |  |























Figure 10
Site Access \& Loop Road Details

COLORADO
Department of Transportation
Region 3

## Transportation Impact Study Methodology Form

Prior to starting a traffic impact study, a Methodology Form must be submitted for review and signed by the Region 3 Access Engineer. It shall be included as part of the study.

Form submitted to CDOT 05/05/20.
CONTACT INFORMATION


## PROJECT INFORMATION

| Project Name | West End |
| :--- | :--- |
| Project Location | Eagle County, CO |
| Project Description <br> (Attached proposed site plan) | See attached plan |
| State Highway | US 6 |
| County | Eagle |
| Mile Post | 166 |
| Posted Speed Limit | 35 mph west of the roundabout |

## TIS ASSUMPTIONS

| Study Years | Current Year: 2020 Buildout | Buildout Year: 2025 | Long Term Year: 2040 |
| :---: | :---: | :---: | :---: |
| Traffic Assessment Level (Provide justification) | Traffic Impact Study |  |  |
| Study Intersections | 1. US 6/Edwards Access Roundabout | 6. |  |
|  | 2. Access Intersections | 7. |  |
|  | 3. | 8. |  |
|  | 4. | 9. |  |
|  | 5. | 10. |  |
| Future Growth Rate | $\square$ OTIS $\quad \square$ Region | $\square$ Regional TDM | $\square$ Other See Notes Section |
| Seasonal Adjustment Factor | March traffic counts will be adjusted to September based on historical seasonal data |  |  |
|  | from CDOT consistent with the Edwards River Park TIA by MCDowell (Factor from March to September is 1.14). |  |  |

## COLORADO

## Department of Transportation

Region 3
ASSUMPTIONS CONTINUED

| Project Trip Distribution (State assumptions and attach sketch that shows individual movements.) | Residential: 25\% west, 35\% north, 30\% east, and 10\% south. Commercial: $25 \%$ west, $30 \%$ north, $25 \%$ east, and $20 \%$ south. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Trip Reduction Percentage | Internal Capture: | N/A |  | Pass By: | 43\% for restaurant uses per ITE Handbook |
|  | Multi-Modal: | N/A |  | Other: | N/A |
| Study Time Periods <br> (Check all that apply) | $\square \mathrm{OM}(7-9)$ 回 PM (4-6) |  |  |  | $\square$ Weekday |
|  | $\square$ SAT (Midday) $\square$ Other |  |  |  |  |
| Existing and Proposed ITE Trip Generation Land Use | Proposed uses will likely be: <br> West End - Apartments/Condos (LUC 220 and/or LUC 221); Vogelman - Apartments/ Condos (LUC 220 and/or LUC 221); Gashouse - Drive-Thru Restaurant (LUC 934) |  |  |  |  |
| Analysis Methods (Check all that apply) | TWSCRoundabouts <br> Synchro or $\quad$ HCS(isolated intersections only) |  |  | $\begin{aligned} & \square \text { SimTraffic or } \square \text { Other } \\ & \text { (closely spaced intersections or when } \\ & \text { known/expected queuing issue) } \end{aligned}$ |  |
|  | $\square$ Signal Warrants |  |  | $\square$ Pedestrian/Transit/Bicycle |  |
|  | $\square$ Safety/Sight Distance |  |  | $\square$ Queuing and Storage |  |
|  | $\square$ Other |  |  |  |  |
| Notes and Other Assumptions | 2025 background traffic will assume Edwards River Park (ERP) is completed plus a background annual growth rate of 0.5 percent. 2040 background traffic will be based on the projections by FHU provided by CDOT in an email dated April 27, 2020 less the site-generated trips assumed by the ERP TIA. |  |  |  |  |
| Crash Data | CDOT will perform a crash data analysis for the highway in the vicinity of the proposed access and provide to the consultant. As a part of the study consultant shall recommend mitigation measures for any identified safety issues. |  |  |  |  |
| Simulation Input Files | Consultant to provide computer files used for analysis with a signed and sealed copy of the study. |  |  |  |  |

## CDOT INTERNAL USE ONLY

Review Comments


Page 2

## Route 006E From 165 to 167



## Legend

—— Route

- Milepoint


## Structures

O Major Structure
O Minor Structure

Created:
Date: 4/3/2020
Time: 12:22:03 PM


The information contained in this map is based on the most currently available data and has been checked for accuracy. CDOT does not guarantee the accuracy of any information presented, is not liable in any respect for any errors or omissions, and is not responsible for determining "fitness for use"


It may appear that information is missing from the straight line diagram. If so, reduce the number of miles/page and re-submit the request.

| ID | Year | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sept | Oct | Nov | Dec |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 11 | 2020 | 25,212 | 24,948 | 20,794 |  |  |  |  |  |  |  |  |  |
| 11 | 2019 | 24,754 | 24,526 | 26,836 | 26,614 | 29,111 | 33,505 | 34,978 | 34,099 | 32,049 | 29,503 | 25,247 | 25,706 |
| 11 | 2018 | 23,833 | 23,879 | 28,066 | 25,227 | 29,140 | 31,990 | 32,973 | 31,668 | 31,171 | 27,693 | 24,967 | 24,944 |
| 11 | 2017 | 21,883 | 23,391 | 27,430 | 24,926 | 27,503 | 32,675 | 33,346 | 31,620 | 29,830 | 27,045 | 25,064 | 24,946 |
| 11 | 2016 | 22,470 | 20,829 | 25,512 | 23,563 | 27,800 | 31,702 | 33,354 | 32,044 | 30,647 | 27,020 | 23,524 | 23,246 |
| 11 | 2015 | 21,420 | 20,606 | 25,633 | 23,457 | 25,290 | 29,571 | 32,273 | 29,663 | 28,616 | 25,758 | 21,938 | 23,347 |
| 11 | 2014 | 19,821 | 19,902 | 23,275 | 21,317 | 23,761 | 27,277 | 29,877 | 28,696 | 26,362 | 24,408 | 20,203 | 21,459 |
| 11 | 2013 | 19,541 | 19,101 | 22,792 | 20,349 | 23,523 | 21,059 | 28,327 | 27,702 | 24,218 | 22,205 | 19,886 | 20,527 |
| 11 | 2012 | 19,531 | 19,755 | 23,271 | 20,611 | 23,037 | 26,496 | 27,976 | 27,526 | 24,666 | 22,125 | 20,449 | 18,208 |
| 11 | 2011 | 18,928 | 18,957 | 21,794 | 19,271 | 21,061 | 25,090 | 27,358 | 27,519 | 25,481 | 22,004 | 19,863 | 20,684 |
| 11 | 2010 | 19,580 | 19,845 | 20,536 | 20,416 | 22,368 | 25,691 | 28,091 | 27,231 | 24,872 | 20,956 | 19,086 | 19,337 |
| 11 | 2009 | 20,473 | 21,084 | 22,687 | 20,734 | 22,971 | 26,494 | 28,787 | 27,696 | 25,134 | 22,138 | 20,205 | 19,814 |
| 11 | 2008 | 21,786 | 22,880 | 24,374 | 22,791 | 24,524 | 26,906 | 28,666 | 28,362 | 25,861 | 23,962 | 20,539 | 19,436 |
| 11 | 2007 | 21,395 | 21,353 | 23,637 | 22,582 | 24,265 | 27,268 | 29,439 | 26,065 | 23,595 | 22,722 | 22,460 | 20,238 |
| 11 | 2006 | 19,845 | 18,485 | 23,220 | 22,153 | 21,138 | 26,740 | 28,011 | 27,524 | 25,338 | 20,618 | 21,992 | 20,939 |
| 11 | 2005 | 19,470 | 21,207 | 22,943 | 21,288 | 23,505 | 27,502 | 26,983 | 26,646 | 24,940 | 22,596 | 20,515 | 19,588 |
| 11 | 2004 | 18,910 | 18,951 | 22,690 | 21,136 | 22,659 | 24,727 | 28,076 | 27,149 | 24,787 | 22,388 | 19,567 | 19,931 |
| 11 | 2003 | 18,431 | 17,949 | 18,942 | 20,692 | 22,441 | 25,869 | 27,729 | 27,381 | 23,831 | 22,323 | 18,017 | 18,767 |
| 11 | 2002 | 17,455 | 18,639 | 20,925 | 20,125 | 22,250 | 23,241 | 25,979 | 25,025 | 21,984 | 21,313 | 18,322 | 19,105 |
| 11 | 2001 |  |  |  |  |  |  |  | 18,732 | 19,138 | 18,973 | 18,976 | 17,924 |

March
2015 to 2019-5 Year Total =
133,477 26,695

## July

2015 to 2019-5 Year Total =

Five Year Average $=$

## September

2015 to 2019-5 Year Total =
152,313
Five Year Average =

## COUNTER MEASURES INC.

1889 YORK STREET
DENVER.COLORADO
$303-333-7409$
N/S STREET: EDWARDS ACCESS RD

[^1]Groups Printed- VEHICLES

|  | EDWARDS ACCESS RDSouthbound |  |  |  | US 6 Westbound |  |  |  | EDWARDS VILLAGE BLVDNorthbound |  |  |  | US 6 Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 6 | 8 | 5 | 0 | 6 | 5 | 9 | 0 | 6 | 16 | 11 | 0 | 18 | 19 | 4 | 0 | 113 |
| 06:45 AM | 19 | 9 | 25 | 0 | 6 | 9 | 7 | 0 | 1 | 29 | 30 | 0 | 33 | 41 | 11 | 0 | 220 |
| Total | 25 | 17 | 30 | 0 | 12 | 14 | 16 | 0 | 7 | 45 | 41 | 0 | 51 | 60 | 15 | 0 | 333 |
| 07:00 AM | 32 | 25 | 20 | 0 | 5 | 9 | 26 | 0 | 1 | 29 | 30 | 0 | 44 | 39 | 11 | 0 | 271 |
| 07:15 AM | 20 | 27 | 22 | 0 | 20 | 26 | 45 | 0 | 6 | 34 | 29 | 0 | 64 | 47 | 16 | 0 | 356 |
| 07:30 AM | 31 | 46 | 49 | 0 | 27 | 29 | 54 | 0 | 8 | 38 | 46 | 0 | 72 | 55 | 23 | 0 | 478 |
| 07:45 AM | 52 | 75 | 94 | 0 | 38 | 46 | 76 | 7 | 5 | 41 | 34 | 0 | 76 | 56 | 24 | 2 | 626 |
| Total | 135 | 173 | 185 | 0 | 90 | 110 | 201 | 7 | 20 | 142 | 139 | 0 | 256 | 197 | 74 | 2 | 1731 |
| 08:00 AM | 35 | 73 | 41 | 0 | 33 | 28 | 63 | 0 | 13 | 32 | 32 | 0 | 82 | 75 | 24 | 0 | 531 |
| 08:15 AM | 39 | 85 | 30 | 0 | 13 | 25 | 29 | 1 | 8 | 14 | 6 | 0 | 33 | 57 | 14 | 0 | 354 |
| Total | 74 | 158 | 71 | 0 | 46 | 53 | 92 | 1 | 21 | 46 | 38 | 0 | 115 | 132 | 38 | 0 | 885 |


| $04: 00 ~ P M ~$ | 55 | 31 | 47 | 0 | 49 | 59 | 53 | 0 | 5 | 58 | 25 | 0 | 51 | 60 | 36 | 0 | 529 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $04: 15 ~ P M$ | 43 | 35 | 51 | 0 | 67 | 54 | 34 | 0 | 7 | 55 | 38 | 0 | 80 | 71 | 44 | 0 | 579 |
| $04: 30$ PM | 37 | 20 | 58 | 0 | 42 | 70 | 40 | 0 | 10 | 62 | 36 | 1 | 89 | 83 | 34 | 0 | 582 |
| $04: 45$ PM | 31 | 27 | 57 | 0 | 50 | 63 | 32 | 0 | 4 | 60 | 50 | 0 | 103 | 77 | 55 | 0 | 609 |
| Total | 166 | 113 | 213 | 0 | 208 | 246 | 159 | 0 | 26 | 235 | 149 | 1 | 323 | 291 | 169 | 0 | 2299 |


| 05:00 PM | 36 | 36 | 67 | 0 | 54 | 78 | 47 | 0 | 7 | 78 | 45 | 0 | 82 | 82 | 72 | 0 | 684 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $05: 15 ~ P M ~$ | 43 | 54 | 80 | 0 | 46 | 80 | 41 | 0 | 5 | 88 | 59 | 0 | 96 | 84 | 58 | 0 | 734 |
| $05: 30 ~ P M ~$ | 29 | 49 | 82 | 0 | 52 | 69 | 28 | 0 | 5 | 97 | 73 | 0 | 88 | 90 | 56 | 0 | 718 |
| $05: 45 \mathrm{PM}$ | 36 | 54 | 61 | 0 | 56 | 72 | 31 | 0 | 3 | 77 | 66 | 0 | 82 | 90 | 59 | 0 | 687 |
| Total | 144 | 193 | 290 | 0 | 208 | 299 | 147 | 0 | 20 | 340 | 243 | 0 | 348 | 346 | 245 | 0 | 2823 |
| Grand Total | 544 | 654 | 789 | 0 | 564 | 722 | 615 | 8 | 94 | 808 | 610 | 1 | 1093 | 1026 | 541 | 2 | 8071 |
| Apprch \% | 27.4 | 32.9 | 39.7 | 0.0 | 29.5 | 37.8 | 32.2 | 0.4 | 6.2 | 53.4 | 40.3 | 0.1 | 41.1 | 38.5 | 20.3 | 0.1 |  |
| Total \% | 6.7 | 8.1 | 9.8 | 0.0 | 7.0 | 8.9 | 7.6 | 0.1 | 1.2 | 10.0 | 7.6 | 0.0 | 13.5 | 12.7 | 6.7 | 0.0 |  |

## COUNTER MEASURES INC.

1889 YORK STREET
DENVER.COLORADO
File Name : EDWAUS6 303-333-7409

Site Code : 00000014
Start Date : 3/4/2020
Page No : 2



## COUNTER MEASURES INC.

1889 YORK STREET
DENVER.COLORADO File Name : EDWAUS6 303-333-7409

Site Code : 00000014
Start Date : 3/4/2020
Page No : 2

|  | EDWARDS ACCESS RD |  |  |  |  | US 6 Westbound |  |  |  |  | EDWARDS VILLAGE BLVD Northbound |  |  |  |  | US 6 <br> Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | $\begin{array}{r} \text { Thr } \\ u \\ \hline \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \\ \hline \end{array}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \\ \hline \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \hline \text { Ped } \\ \mathrm{s} \\ \hline \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \\ \hline \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \hline \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \\ \hline \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \\ \hline \end{array}$ | App. Total | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |
| Peak Hour From 04:00 PM to 05:45 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersecti on | 05:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Volume | 144 | 193 | 290 | 0 | 627 | 208 | 299 | 147 | 0 | 654 | 20 | 340 | 243 | 0 | 603 | 348 | 346 | 245 | 0 | 939 | 2823 |
| Percent | $\begin{array}{r} 23 . \\ 0 \end{array}$ | $\begin{array}{r} 30 . \\ 8 \end{array}$ | $\begin{array}{r} 46 . \\ 3 \end{array}$ | 0.0 |  | $31 .$ $8$ | $45 \text {. }$ | $\begin{array}{r} 22 . \\ 5 \end{array}$ | 0.0 |  | 3.3 | $56 .$ $4$ | $\begin{array}{r} 40 . \\ 3 \end{array}$ | 0.0 |  | $37 .$ $1$ | $\begin{array}{r} 36 . \\ 8 \end{array}$ | $26$ $1$ | 0.0 |  |  |
| $05: 15$ | 43 | 54 | 80 | 0 | 177 | 46 | 80 | 41 | 0 | 167 | 5 | 88 | 59 | 0 | 152 | 96 | 84 | 58 | 0 | 238 | 734 |
| Peak | 05:15 PM |  |  |  |  | 05:00 PM |  |  |  |  | 05:30 PM |  |  |  |  | 05:15 PM |  |  |  |  |  |
| Factor |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| High Int. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Volume | 43 | 54 | 80 | 0 | 177 |  |  |  |  |  | 54 | 78 | 47 | 0 | 179 | 5 | 97 | 73 | 0 | 175 | 96 | 84 | 58 | 0 | 238 |  |
| Peak |  |  |  |  | 0.88 |  |  |  |  |  |  |  |  |  | 0.91 |  |  |  |  | 0.86 |  |  |  |  | 0.98 |  |
| Factor |  |  |  |  | 6 |  |  |  |  | 3 |  |  |  |  | 1 |  |  |  |  | 6 |  |



## COUNTER MEASURES INC.

1889 YORK STREET
DENVER.COLORADO File Name : EDW ACC RD WELLS F-B 303-333-7409

Site Code : 00000014
Start Date: 3/5/2020
Page No : 1
Groups Printed- VEHICLES
BUS ACC N/OUS

|  | EDWARDS ACCESS RD Southbound |  |  |  | WELLS FARGO ACC Westbound |  |  |  | EDWARDS ACCESS RD Northbound |  |  |  | BUS ACC N/O US-6 Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 5 |
| 06:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 15 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 1 | 0 | 20 |


| 07:00 AM | 0 | 0 | 1 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 14 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | :--- | :--- | :--- | :--- | :--- |
| $07: 15 \mathrm{AM}$ | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 13 |
| $07: 30$ AM | 0 | 0 | 2 | 0 | 0 | 0 | 14 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 2 | 0 | 21 |
| $07: 45$ AM | 0 | 0 | 1 | 0 | 0 | 0 | 24 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 3 | 0 | 33 |
| Total | 0 | 0 | 4 | 0 | 0 | 0 | 56 | 0 | 0 | 0 | 14 | 0 | 0 | 0 | 7 | 0 | 81 |


| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 0 | 0 | 12 | 1 | 0 | 0 | 1 | 0 | 28 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 08:15 AM | 0 | 0 | 1 | 0 | 0 | 0 | 20 | 0 | 0 | 0 | 13 | 2 | 0 | 0 | 0 | 0 | 36 |
| Total | 0 | 0 | 1 | 0 | 0 | 0 | 34 | 0 | 0 | 0 | 25 | 3 | 0 | 0 | 1 | 0 | 64 |


| 04:00 PM | 0 | 0 | 1 | 0 | 0 | 0 | 31 | 0 | 0 | 0 | 26 | 0 | 0 | 0 | 3 | 0 | 61 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 42 | 0 | 0 | 0 | 25 | 0 | 0 | 0 | 1 | 0 | 68 |
| 04:30 PM | 0 | 0 | 2 | 0 | 0 | 0 | 85 | 0 | 0 | 0 | 33 | 0 | 0 | 0 | 4 | 0 | 124 |
| 04:45 PM | 0 | 0 | 1 | 0 | 0 | 0 | 106 | 0 | 0 | 0 | 21 | 0 | 0 | 0 | 4 | 0 | 132 |
| Total | 0 | 0 | 4 | 0 | 0 | 0 | 264 | 0 | 0 | 0 | 105 | 0 | 0 | 0 | 12 | 0 | 385 |


| 05:00 PM | 0 | 0 | 1 | 0 | 0 | 0 | 121 | 0 | 0 | 0 | 26 | 0 | 0 | 0 | 2 | 0 | 150 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 0 | 33 | 0 | 0 | 0 | 5 | 0 | 138 |
| 05:30 PM | 0 | 0 | 2 | 0 | 0 | 0 | 135 | 0 | 0 | 0 | 28 | 0 | 0 | 0 | 4 | 0 | 169 |
| 05:45 PM | 0 | 0 | 1 | 0 | 0 | 0 | 115 | 0 | 0 | 0 | 31 | 0 | 0 | 0 | 6 | 0 | 153 |
| Total | 0 | 0 | 4 | 0 | 0 | 0 | 471 | 0 | 0 | 0 | 118 | 0 | 0 | 0 | 17 | 0 | 610 |


| Grand Total | 0 | 0 | 13 | 0 | 0 | 0 | 838 | 0 | 0 | 0 | 268 | 3 | 0 | 0 | 38 | 0 | 1160 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Apprch \% | 0.0 | 0.0 | 100.0 | 0.0 | 0.0 | 0.0 | 100.0 | 0.0 | 0.0 | 0.0 | 98.9 | 1.1 | 0.0 | 0.0 | 100.0 | 0.0 |  |
| Total \% | 0.0 | 0.0 | 1.1 | 0.0 | 0.0 | 0.0 | 72.2 | 0.0 | 0.0 | 0.0 | 23.1 | 0.3 | 0.0 | 0.0 | 3.3 | 0.0 |  |

## COUNTER MEASURES INC.

1889 YORK STREET
DENVER.COLORADO 303-333-7409

File Name : EDW ACC RD WELLS F-B
Site Code : 00000014
Start Date : 3/5/2020
Page No : 2

|  | EDWARDS ACCESS RDSouthbound |  |  |  |  | WELLS FARGO ACC <br> Westbound |  |  |  |  | EDWARDS ACCESS RD Northbound |  |  |  |  | BUS ACC N/O US-6Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | Left | Thr u | $\begin{gathered} \text { Rig } \\ \text { ht } \end{gathered}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | Thr | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | Ped s | App. Total | $\begin{gathered} \text { Int. } \\ \text { Total } \end{gathered}$ |

Peak Hour From 07:15 AM to 08:00 AM - Peak 1 of 1


|  |  |  |
| :---: | :---: | :---: |
|  |  |  |
|  |  |  |

## COUNTER MEASURES INC.

1889 YORK STREET
DENVER.COLORADO 303-333-7409

File Name : EDW ACC RD WELLS F-B
Site Code : 00000014
Start Date : 3/5/2020
Page No : 2

|  | EDWARDS ACCESS RDSouthbound |  |  |  |  | WELLS FARGO ACC <br> Westbound |  |  |  |  | EDWARDS ACCESS RDNorthbound |  |  |  |  | BUS ACC N/O US-6Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{gathered} \text { Rig } \\ \mathrm{ht} \end{gathered}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | Thr u | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \hline \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | Thr | $\begin{gathered} \mathrm{Rig} \\ \mathrm{ht} \end{gathered}$ | Ped s | App. Total | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |

Peak Hour From 04:00 PM to 05:45 PM - Peak 1 of 1

| Intersecti | 05:00 | PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 471 | 0 | 471 | 0 | 0 | 118 | 0 | 118 | 0 | 0 | 17 | 0 | 17 | 610 |
| Percent | 0.0 | 0.0 | 100 .0 | 0.0 |  |  | 0.0 | 100 .0 | 0.0 |  |  |  | 100 .0 | 0.0 |  | 0.0 | 0.0 | 100 .0 | 0.0 |  |  |
| 05:30 <br> Volume Peak | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 135 | 0 | 135 | 0 | 0 | 28 | 0 | 28 | 0 | 0 | 4 | 0 | 4 | $\begin{aligned} & 169 \\ & 0.902 \end{aligned}$ |
| Factor |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| High Int. | 05:30 | PM |  |  |  | 05:30 | PM |  |  |  | 05:15 | PM |  |  |  | 05:45 | PM |  |  |  |  |
| Volume | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 135 | 0 | 135 | 0 | 0 | 33 | 0 | 33 | 0 | 0 | 6 | 0 | 6 |  |
| Peak |  |  |  |  | 0.50 |  |  |  |  | 0.87 |  |  |  |  | 0.89 |  |  |  |  | 0.70 |  |
| Factor |  |  |  |  | 0 |  |  |  |  | 2 |  |  |  |  | 4 |  |  |  |  | 8 |  |



COUNTER MEASURES INC.
1889 YORK STREET
DENVER.COLORADO File Name : EDW ACC ALPINE ACC-B
N/S STREET: EDWARDS ACC RD 303-333-7409
E/W STREET: ALPINE BANK ACC RD CITY: EDWARDS
COUNTY: EAGLE
Site Code : 00000000
Start Date : 3/4/2020
Page No : 1
Groups Printed- VEHICLES

|  | EDWARDS ACC RDSouthbound |  |  |  | Westbound |  |  |  | EDWARDS ACC RDNorthbound |  |  |  | ALPINE BANK ACC Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | $\begin{aligned} & \text { Int. } \\ & \text { Total } \end{aligned}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 06:45 AM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| Total | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |


| 07:00 AM | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 7 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 07:15 AM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 5 |
| 07:30 AM | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 12 |
| 07:45 AM | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 9 |
| Total | 0 | 0 | 7 | 4 | 0 | 0 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 9 | 1 | 33 |


| 08:00 AM | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $08: 15$ AM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 11 |



| 04:00 PM | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 3 | 0 | 0 | 24 | 0 | 43 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 04:15 PM | 0 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 21 | 0 | 0 | 4 | 0 | 0 | 36 | 0 | 74 |
| 04:30 PM | 0 | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 0 | 2 | 0 | 0 | 41 | 0 | 73 |
| 04:45 PM | 0 | 0 | 23 | 0 | 0 | 0 | 0 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 51 | 0 | 93 |
| Total | 0 | 0 | 65 | 0 | 0 | 0 | 0 | 0 | 57 | 0 | 0 | 9 | 0 | 0 | 152 | 0 | 283 |


| 05:00 PM | 0 | 0 | 18 | 0 | 0 | 0 | 0 | 0 | 18 | 0 | 0 | 5 | 0 | 0 | 48 | 0 | 89 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $05: 15 ~ P M ~$ | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 23 | 0 | 0 | 6 | 0 | 0 | 50 | 0 | 93 |
| $05: 30 ~ P M ~$ | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 26 | 0 | 0 | 3 | 0 | 0 | 28 | 0 | 67 |
| $05: 45 \mathrm{PM}$ | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 39 | 0 | 71 |
| Total | 0 | 0 | 54 | 0 | 0 | 0 | 0 | 0 | 87 | 0 | 0 | 14 | 0 | 0 | 165 | 0 | 320 |


| Grand Total | 0 | 0 | 135 | 4 | 0 | 0 | 0 | 0 | 179 | 0 | 0 | 23 | 0 | 0 | 327 | 1 | 669 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Apprch \% | 0.0 | 0.0 | 97.1 | 2.9 | 0.0 | 0.0 | 0.0 | 0.0 | 88.6 | 0.0 | 0.0 | 11.4 | 0.0 | 0.0 | 99.7 | 0.3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total \% | 0.0 | 0.0 | 20.2 | 0.6 | 0.0 | 0.0 | 0.0 | 0.0 | 26.8 | 0.0 | 0.0 | 3.4 | 0.0 | 0.0 | 48.9 | 0.1 |

## COUNTER MEASURES INC.

1889 YORK STREET
DENVER.COLORADO 303-333-7409

File Name : EDW ACC ALPINE ACC-B
Site Code : 00000000
Start Date : 3/4/2020
Page No : 2

|  | EDWARDS ACC RD Southbound |  |  |  |  | Westbound |  |  |  |  | EDWARDS ACC RDNorthbound |  |  |  |  | ALPINE BANK ACC Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{gathered} \text { Rig } \\ \text { ht } \end{gathered}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r\|} \hline \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{gathered} \text { Rig } \\ \mathrm{ht} \end{gathered}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | Ped s | App. Total | Int. Total |

Peak Hour From 07:15 AM to 08:00 AM - Peak 1 of 1


|  |  |  |
| :---: | :---: | :---: |
|  |  |  |
|  |  |  |

## COUNTER MEASURES INC.

1889 YORK STREET
DENVER.COLORADO 303-333-7409

File Name : EDW ACC ALPINE ACC-B
Site Code : 00000000
Start Date : 3/4/2020
Page No : 2

|  | EDWARDS ACC RDSouthbound |  |  |  |  | Westbound |  |  |  |  | EDWARDS ACC RDNorthbound |  |  |  |  | ALPINE BANK ACC Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | Left | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | $\begin{gathered} \text { Rig } \\ \mathrm{ht} \end{gathered}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{gathered} \text { Rig } \\ \mathrm{ht} \end{gathered}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | Ped s | App. Total | $\begin{gathered} \text { Int. } \\ \text { Total } \end{gathered}$ |

Peak Hour From 05:00 PM to 05:45 PM - Peak 1 of 1


|  |  |  |
| :---: | :---: | :---: |
|  |  |  |
|  |  |  |

## COUNTER MEASURES INC.

File Name: 2ND ACC W-O RND US 6-B
N/S STREET: US-6
Site Code : 00000011
Start Date: 3/4/2020
Page No : 1 CITY: EDWARDS
COUNTY: EAGLE
Groups Printed- VEHICLES

|  | Southbound |  |  |  | US-6 Westbound |  |  |  | 2ND ACC W/O RND A BOUT Northbound |  |  |  | US-6 <br> Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 06:45 AM | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 3 | 0 | 2 | 0 | 0 | 0 | 1 | 1 | 12 |
| Total | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 3 | 0 | 2 | 0 | 0 | 0 | 1 | 1 | 13 |


| 07:00 AM | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 3 | 0 | 8 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 07:15 AM | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 3 | 0 | 7 | 0 | 0 | 0 | 3 | 3 | 18 |
| 07:30 AM | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 5 |
| 07:45 AM | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 6 | 0 | 4 | 0 | 0 | 0 | 6 | 2 | 29 |
| Total | 0 | 0 | 0 | 0 | 19 | 0 | 0 | 0 | 9 | 0 | 14 | 0 | 0 | 0 | 13 | 5 | 60 |
| 08:00 AM | 0 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 8 | 1 | 25 |
| Total | 0 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 8 | 1 | 25 |


| 04:00 PM | 0 | 0 | 0 | 0 | 21 | 0 | 0 | 0 | 7 | 0 | 18 | 0 | 0 | 0 | 5 | 3 | 54 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 04:15 PM | 0 | 0 | 0 | 0 | 25 | 0 | 0 | 0 | 13 | 0 | 32 | 0 | 0 | 0 | 11 | 2 | 83 |
| 04:30 PM | 0 | 0 | 0 | 0 | 18 | 0 | 0 | 0 | 8 | 0 | 20 | 0 | 0 | 0 | 5 | 0 | 51 |
| 04:45 PM | 0 | 0 | 0 | 0 | 27 | 0 | 0 | 1 | 8 | 0 | 22 | 0 | 0 | 0 | 7 | 2 | 67 |
| Total | 0 | 0 | 0 | 0 | 91 | 0 | 0 | 1 | 36 | 0 | 92 | 0 | 0 | 0 | 28 | 7 | 255 |


| 05:00 PM | 0 | 0 | 0 | 0 | 19 | 0 | 0 | 0 | 14 | 0 | 20 | 0 | 0 | 0 | 6 | 5 | 64 |
| ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | ---: | ---: | ---: |
| $05: 15 \mathrm{PM}$ | 0 | 0 | 0 | 0 | 29 | 0 | 0 | 0 | 10 | 0 | 18 | 0 | 0 | 0 | 4 | 2 | 63 |
| $05: 30 \mathrm{PM}$ | 0 | 0 | 0 | 0 | 12 | 0 | 0 | 0 | 15 | 0 | 17 | 0 | 0 | 0 | 6 | 0 | 50 |
| $05: 45 \mathrm{PM}$ | 0 | 0 | 0 | 0 | 24 | 0 | 0 | 0 | 14 | 0 | 13 | 0 | 0 | 0 | 4 | 0 | 55 |
| Total | 0 | 0 | 0 | 0 | 84 | 0 | 0 | 0 | 53 | 0 | 68 | 0 | 0 | 0 | 20 | 7 | 232 |


| Grand Total | 0 | 0 | 0 | 0 | 209 | 0 | 0 | 1 | 101 | 0 | 183 | 0 | 0 | 0 | 70 | 21 | 585 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Apprch \% | 0.0 | 0.0 | 0.0 | 0.0 | 99.5 | 0.0 | 0.0 | 0.5 | 35.6 | 0.0 | 64.4 | 0.0 | 0.0 | 0.0 | 76.9 | 23.1 |  |
| Total \% | 0.0 | 0.0 | 0.0 | 0.0 | 35.7 | 0.0 | 0.0 | 0.2 | 17.3 | 0.0 | 31.3 | 0.0 | 0.0 | 0.0 | 12.0 | 3.6 |  |

## COUNTER MEASURES INC.

1889 YORK STREET
N/S STREET: US-6
DENVER.COLORADO
File Name: 2ND ACC W-O RND US 6-B
E/W STREET: 2ND ACC W/O RND A BOUT 303-333-7409

Site Code : 00000011
Start Date: 3/4/2020
Page No : 2



## COUNTER MEASURES INC.

1889 YORK STREET

N/S STREET: US-6
E/W STREET: 2ND ACC W/O RND A BOUT CITY: EDWARDS
COUNTY: EAGLE

File Name : 2ND ACC W-O RND US 6-B
Site Code : 00000011
Start Date : 3/4/2020
Page No : 2

|  | Southbound |  |  |  |  | US-6 <br> Westbound |  |  |  |  | 2ND ACC W/O RND A BOUT Northbound |  |  |  |  | US-6 <br> Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \hline \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{gathered} \text { Rig } \\ \text { ht } \end{gathered}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{gathered} \text { Rig } \\ \text { ht } \end{gathered}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. <br> Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{gathered} \mathrm{Rig} \\ \mathrm{ht} \end{gathered}$ | $\begin{array}{r} \hline \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{aligned} & \text { Int. } \\ & \text { Total } \end{aligned}$ |

Peak Hour From 05:00 PM to 05:45 PM - Peak 1 of 1


## COUNTER MEASURES INC.

1889 YORK STREET
N/S STREET: 1ST ACC W-O RND
DENVER.COLORADO 303-333-7409

File Name: 1ST ACC W-O RND US 6
E/W STREET: US-6
CITY: EDWARDS
COUNTY: EAGLE
Site Code : 00000011
Start Date : 3/4/2020
Page No : 1
Groups Printed- IST ACC W-O RND US-6
US 6

|  | 1ST ACC W-O RND Southbound |  |  |  | US 6 <br> Westbound |  |  |  | Northbound |  |  |  | US 6 Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Int. Total |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |


| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:00 PM | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 05:15 PM | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 05:30 PM | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Total | 0 | 0 | 4 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| Grand Total | 0 | 0 | 4 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| Apprch \% | 0.0 | 0.0 | 100.0 | 0.0 | 0.0 | 0.0 | 100.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total \% | 0.0 | 0.0 | 36.4 | 0.0 | 0.0 | 0.0 | 63.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |

## COUNTER MEASURES INC

1889 YORK STREET
DENVER.COLORADO 303-333-7409

File Name : 1ST ACC W-O RND US 6
Site Code : 00000011
Start Date: 3/4/2020
Page No : 2

|  | 1ST ACC W-O RND Southbound |  |  |  |  | US 6 <br> Westbound |  |  |  |  | Northbound |  |  |  |  | US 6 Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \mathrm{Ped} \\ \mathrm{~s} \end{array}$ | App. Total | Left | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | Rig ht | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\mathrm{Rig}$ | $\begin{array}{r} \mathrm{Ped} \\ \mathrm{~s} \end{array}$ | App. Total | Left | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \mathrm{Ped} \\ \mathrm{~s} \end{array}$ | App. Total | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |

Peak Hour From 06:30 AM to 08:15 AM - Peak 1 of 1



## COUNTER MEASURES INC.

1889 YORK STREET
DENVER.COLORADO 303-333-7409

File Name: 1ST ACC W-O RND US 6
Site Code : 00000011
Start Date: 3/4/2020
Page No : 2

|  | 1ST ACC W-O RND Southbound |  |  |  |  | US 6 Westbound |  |  |  |  | Northbound |  |  |  |  | US 6 Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | Left | $\begin{gathered} \text { Thr } \\ \mathrm{u} \end{gathered}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{gathered} \mathrm{Rig} \\ \mathrm{ht} \end{gathered}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{gathered} \text { Rig } \\ \text { ht } \end{gathered}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{gathered} \mathrm{Thr} \\ \mathrm{u} \end{gathered}$ | $\begin{array}{r} \text { Rig } \\ \text { ht } \end{array}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{aligned} & \text { Int. } \\ & \text { Total } \end{aligned}$ |

Peak Hour From 04:00 PM to 05:45 PM - Peak 1 of 1

| Intersecti on <br> Volume | 05:00 | PM | 4 | 0 | 4 | 0 | 0 | 6 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Percent | 0.0 | 0.0 | $100$ | 0.0 |  | 0.0 | 0.0 | 100 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| 05:30 Peak | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\begin{gathered} 3 \\ 0.833 \end{gathered}$ |
| High Int. | 05:30 | PM |  |  |  | 05:00 | PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Volume Peak Factor | 0 | 0 | 2 | 0 | 2 0.50 0 | 0 | 0 | 2 | 0 | 2 0.75 0 |  |  |  |  |  |  |  |  |  |  |  |



### 3.0 Future Traffic Projections

### 3.1 Background Infrastructure Assumptions

Eagle County and CDOT have begun construction in February 2019 on a new roundabout at the intersection of US 6 and I-70G. The roundabout is anticipated to be completed in Year 2019. Therefore, the Year 2022 and Year 2040 analyses incorporate the new roundabout based upon construction plans provided by Eagle County.

### 3.2 Seasonal Adjustment Factor

Traffic data was collected in January 2019. School was in session. Based upon data obtained from CDOT's Automatic Traffic Recorders (ATRs), traffic volumes in September are higher than any other time of year; except for the peak season summer months of June, July and August. Therefore, a seasonal adjustment factor of 1.26 was applied to all of the traffic counts to adjust the January counts to September volumes. The seasonal adjustment factor calculations from the ATR are included in the Appendix. This methodology is consistent with the Maintenance Study and the I-70 $G$ study.

### 3.3 Background Traffic Growth

This project was originally scoped to use CDOT's historic growth rates on US 6 and I70G. Per CDOT, the US 6 corridor near the project site is anticipated to have a 20 -year growth factor of 1.47 , which equates to a $1.94 \%$ annual growth rate at the project site.

However, during the analysis, it was determined that this methodology was not consistent with the Maintenance Study and I-70G Study. Forecasting at CDOT's historic growth rates yield significantly lower traffic projections than the methodology used in the Maintenance Study and I-70G Study.

Therefore, future background traffic growth was modeled using a base $1.00 \%$ growth rate and adding in approved project traffic that will contribute to the US 6 and I-70G corridors. This methodology is consistent with the Maintenance Study and the I-70 G study. Unlike the previous studies, the $1.00 \%$ base growth rate was applied to all movements at the study intersections. The previous studies have assumed that Edwards Village Boulevard is not experiencing traffic growth. Based upon current count data, that is not the case. The base growth rate was also applied to Lake Creek Road movements.

There are a number of developments planned for the Edwards area, including: the West End/Vogelman properties; Eagle River Meadows; Cordillera, and others. The traffic increase associated with these developments was obtained from the I-70G Study, with updated information for the projects that have been modified since the I70G Study was done. The previously approved projects included in the growth
projections are summarized below in Table 1. The forecast comparison is depicted in Figure 3

Table 1: Approved Projects - Background Trip Generation Calculations

| Development | Land Use | Size | Average Weekday | AM Peak Hour Traffic |  |  | PM Peak Hour Traffic |  |  | SAT Peak Hour Traffic ${ }^{4}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Trips | In | Out | Total | In | Out | Total | In | Out | Total |
| East of Eagle River Park: |  |  |  |  |  |  |  |  |  |  |  |  |
| West End/Vogelman | Commercial (A) ${ }^{3}$ | 100 ksf | 4270 | 60 | 35 | 95 | 180 | 190 | 370 | 234 | 216 | 450 |
|  | MF Residential (B) ${ }^{3}$ | 200 du | 1330 | 20 | 80 | 100 | 80 | 45 | 125 | 83 | 57 | 140 |
| Subtotal - Projects East of ERP |  |  | 5600 | 80 | 115 | 195 | 260 | 235 | 495 | 317 | 273 | 590 |
| West of Eagle River Park: |  |  |  |  |  |  |  |  |  |  |  |  |
| Cordillera | SF Residential (C) ${ }^{3}$ | 350 du | 3330 | 65 | 195 | 260 | 220 | 130 | 350 | 168 | 144 | 312 |
| Fox Hollow | MF Residential (B) ${ }^{1}$ | 90 du | 497 | 8 | 30 | 38 | 28 | 16 | 44 | 45 | 39 | 84 |
| Six West (VIA) | MF Residential (B) ${ }^{2}$ | 121 du | 768 | 18 | 46 | 64 | 48 | 29 | 77 | 61 | 52 | 113 |
| Stillwater | MF Residential (B) | 21 du | 138 | 2 | 9 | 11 | 9 | 5 | 14 | 11 | 9 | 20 |
| Subtotal - Projects West of ERP |  |  | 4,733 | 93 | 280 | 373 | 305 | 180 | 485 | 285 | 244 | 529 |
| Projects on I-70G: |  |  |  |  |  |  |  |  |  |  |  |  |
| North Star | Commercial (1) ${ }^{3}$ | 23 ksf | 980 | 15 | 5 | 20 | 40 | 45 | 85 | 54 | 50 | 104 |
| Subtotal - Projects on I-70G |  |  | 980 | 15 | 5 | 20 | 40 | 45 | 85 | 54 | 50 | 104 |
| Total Approved Development |  |  | 11,313 | 188 | 400 | 588 | 605 | 460 | 1,065 | 656 | 567 | 1,223 |

A. ITE Land Use Code 820 Shopping Center
B. ITE Land Use Code 220 Multifamily
C. ITE Land Use Code 210 Single Family Detached Housing
${ }^{1}$ Data from Fox Hollow Transportation Impact Study.
${ }^{2}$ Data from Six West Transportation Impact Study.
${ }^{3}$ Data from FHU's I-70G and US 6 Roundabout Traffic Study.
${ }^{4}$ Data from ITE Trip Generation, 10 th Edition.
Note: The Hagedorn mini storage facility has been in full operations at the time of traffic data collection.

These trips were assigned to the study area roadways based on trip distribution patterns established in previous traffic engineering documents (I-70G Study, Edwards Area Access Control Plan, and US 6 and I-70 G Corridor Feasibility Study), as follows:

- 25 percent oriented to/from US 6 west of the Edwards Area
- 30 percent oriented to/from US 6 east of the Edwards Area
- 45 percent oriented to/from I-70 north of the study area

Per the I-70G Study, "Most of the above development is located west of the US 6/I-70 G intersection; therefore, only 75 percent of the trips generated within these developments would impact the study area roadways (the remaining 25 percent would be oriented to/from the west via US 6). All of the North Star development generated traffic would impact study area intersections, with 45 percent oriented to/from the north via I-70 G; thus, only 55 percent of North Star traffic would impact the US 6/I-70 G intersection ( 25 percent to/from the west and 30 percent to from the east via US 6)."

## MEMORANDUM

TO: Michelle Stevens<br>FROM: Charles Buck<br>DATE: May 15, 2019<br>SUBJECT: Review of Transportation Impact Study for Edwards River Park McDowell Engineering<br>FHU Reference No, II 2475-07

I have reviewed the McDowell report for Edwards River Park, dated March 25, 2019. Both CDOT and Eagle County have expressed concerns that the projections contained within this report are substantially higher than the design volumes we developed for the I-70 G Edwards Interchange Upgrade Phase 2 effort in 2016. Although our methods, assumptions, and resultant projections were vetted through the design team, recent traffic counts and analyses conducted by McDowell Engineering (McD) suggest that our projections may have underestimated the growth potential in the Edwards area. Therefore, to better understand how the McD projections were developed, I have reviewed the methods, assumptions, and calculations of the 2040 traffic volume forecasts at the US 6 and I-70 G intersection.

The intent of this review is to establish appropriate design volumes for the intersection. Note that McD considers a Saturday scenario in addition to weekday forecasts; I have focused my analysis on the weekday scenario for consistency with our 2016 study. I have the following comments:

## Methods

I. The McD projections are based on traffic counts conducted January 29, 2019. These counts are substantially higher than the adjusted existing traffic volumes we developed for our report. The McD data include school related traffic.
2. The McD report adjusted the traffic counts using a Seasonal Adjustment Factor (SAF) calculated from CDOT Continuous Count data for I-70 at Wolcott (there are no continuous counters on US 6 near Edwards). The counts were adjusted to represent September using a factor of I.26.
3. The McD report then factored these volumes by an annual growth rate of one percent per year to 2040. This is generally consistent with how we grew our background traffic volumes.
4. McD then added in traffic generated by potential developments in the Edwards area, which is also generally consistent with our methodology. McD also updated some of the future developments, as proposed densities have changed since 2016.
5. Trips generated by Edwards River Park (the proposed development which is the subject of the McD report) were then added in. The proposed land uses and densities for Edwards River Park (ERP) have also changed since 2016.

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## Differences from FHU Report

I. As noted above, the McD counts are higher than FHU's. We conducted our counts in June 2015, then adjusted them to reflect both the September 2015 recounts and August 2015 Stolfus counts (see Edwards Transportation and Maintenance Analysis Study).
2. The McD traffic counts were further increased using the $I .26$ SAF. The SAF is based on I-70 regional travel patterns, which may or may not reflect the more localized travel along US 6 through Edwards.
3. McD applied the 1.0 percent annual growth rate to all study area movements. FHU applied this regional rate only to regional movements; local traffic increases were accounted for in the trip generation analysis of future development in Edwards.
4. McD applied the $I .0$ percent growth rate to Edwards Village Boulevard (EVB) volumes, while FHU did not, as this roadway does not serve regional traffic movements.
5. The background development in Edwards has increased in density. Comparing McD Table I to FHU Table I (and extracting FHU's estimates for Eagle River Meadows (now ERP), the increases due to higher densities are 70 to 80 vehicles per hour ( 835 trips per day).
6. The trip generation for ERP has increased as well, due to the current mix of residential and commercial uses proposed. Comparing McD Table 6 to Eagle River Meadows in the FHU Table I, the increases are about 240 to 360 vehicles per hour, and 3,500 trips per day. These increases more than double our previous trip generation estimates for the ERP site.

## Analysis

I. The January 2019 traffic counts clearly show that traffic has grown since the 2015 counts were conducted, and at a higher rate than would be calculated assuming a straight-line growth from 2015 to 2040 .
2. The McD projections may be overly conservative. The SAF of $I .26$ adjusts the January volumes to September, which is a peak month. Adjusting to the annual average may be more appropriate for design; the SAF for the annual average is I.I6, based on the I-70 continuous counter data. Also, McD applied the SAF to Edwards Village Boulevard. As EVB serves primarily local traffic, it should be generally unaffected by regional fluctuations (other than school-related peaking, which is already accounted for in the data).
3. McD applied the $I .0$ percent regional growth factor to EVB. However, lands served by EVB are generally built out. The only potential development remaining is "Tract T", a four-acre commercial site located southwest and up the hill from Edwards Corner. Tract T was not included in our 2016 analysis per direction from Eagle County. It is estimated, however, that this site could develop with about 43,000 square feet of office/business park type uses. A trip generation analysis assuming office yields an increase of about 50 trips during either peak hour, far less than McD calculated using the 1.0 percent annual growth factor.

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4. For perspective, the overall annual growth rates (AGR) implied by the McD report (2019 to 2040 total) are between 3.8 percent (AM) and 4.7 percent (PM) along US 6, which is 3 to 4 times higher than CDOT's historic growth rate of 1.3 percent per year (calculated from the 20-year factor on OTIS). The McD rates are between 3.0 and 3.5 percent on $\mathrm{I}-70 \mathrm{G}$, about three times higher compared to 1.03 percent per OTIS.
5. The trip generation for ERP, as shown in McD Table 6, introduces an error via the internal capture reductions. The internal trips assigned to the commercial ( 35 percent), spa/restaurant ( 50 percent), conference center ( 80 percent), and amphitheater/wedding venue ( 20 percent) total more than the residential and hotel uses can account for. The reductions estimated by McD are summarized in the following table:

## Internal Trips - Edwards River Park - McD Report

| Commercial Trip Reductions |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | AM Peak Hour |  | PM Peak Hour |  |  |  |  |  |
|  | In | Out | In | Out |  |  |  |  |
| Shopping Center | -40 | -34 | -58 | -58 |  |  |  |  |
| Hotel Spa/Restaurant | -16 | -7 | -18 | -15 |  |  |  |  |
| Conference Center | -137 | -25 | -25 | -137 |  |  |  |  |
| Amphitheatre/Wedding | 0 | 0 | -6 | 0 |  |  |  |  |
| Total Reductions | $-\mathbf{- 1 9 3}$ | $\mathbf{- 6 6}$ | $\mathbf{- 1 0 7}$ | $\mathbf{- 2 1 0}$ |  |  |  |  |
| Residential Vehicle Trips |  |  |  |  |  |  |  |  |
| Lan Peak Hour | PM Peak Hour |  |  |  |  |  |  |  |
|  | In |  |  |  |  |  | Out | In | Out |
| Residential | 35 | 141 | 123 | 69 |  |  |  |  |
| Hotel | 33 | 29 | 34 | 54 |  |  |  |  |
| Total Vehicle Trips | $\mathbf{6 8}$ | $\mathbf{1 7 0}$ | $\mathbf{1 5 7}$ | $\mathbf{7 4}$ |  |  |  |  |

In looking at the above table, consider the following internal trip directionality:

- An inbound trip to the commercial uses is outbound from the residential uses.
- An outbound trip from the commercial is inbound to the residential.

It can be seen that inbound commercial in the AM exceeds the outbound residential trip generation by 23 trips. The outbound commercial to residential is only 2 trips less than the residential inbound trip generation. In the PM peak hour, the internal commercial trips exceed the residential trips in both directions. Thus, the McD internal trip generation assumptions are simply not possible. Also, McD does not actually reduce the residential trips - only the commercial; this is an unrealistic approach.

A more rational way to model the internal capture would be to reduce the residential trips by an appropriate percentage with a reciprocal reduction in the commercial trips. I have estimated that maybe 50 percent of the residential trips could be captured by the commercial uses at ERP. The following table demonstrates the resultant reductions:

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Internal Trips - Edwards River Park - FHU Estimates

| Residential Trips |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Trip Type | AM Peak Hour |  | PM Peak Hour |  |
|  | In | Out | In | Out |
| Total Residential Trips | 70 | 170 | 155 | 125 |
| Internal Trips | $\mathbf{- 3 5}$ | $\mathbf{- 8 5}$ | $\mathbf{- 7 5}$ | $\mathbf{- 6 5}$ |
| External Trips | 35 | 85 | 80 | 60 |
| Commercial Trips |  |  |  |  |
| Trip Type | AM Peak Hour | PM Peak Hour |  |  |
|  | In | Out | In | Out |
|  | 315 | 140 | 510 | 370 |
|  | $\mathbf{- 8 5}$ | $\mathbf{- 3 5}$ | $\mathbf{- 6 5}$ | $\mathbf{- 7 5}$ |
|  | 230 | 105 | 445 | 295 |
|  | $\mathbf{2 6 5}$ | $\mathbf{1 9 0}$ | $\mathbf{5 2 5}$ | $\mathbf{3 5 5}$ |
| Note: volumes are rounded to the nearest 5 for simplicity. |  |  |  |  |

By comparing the above table to McD Table I, it can be seen that the McD report may be underestimating the trip generation potential of ERP and its consequent impacts on area roadways. The inbound/outbound directionality of the external trips is also affected.

## Proposed Traffic Volume Revisions (see attached Figures)

I. I have used the January 2019 traffic counts as the basis for updating the 2040 projections (Figure I).
2. These volumes are increased using an annual average SAF of 1.16 (Figure 2). The SAF is not applied to Edwards Village Boulevard, which serves primarily local users.
3. The 1.0 percent per year regional growth rate is applied to regional movements (Figure 3). This AGR is also not applied to EVB. To account for future growth on EVB, the Tract T trip generation (Figure $\boldsymbol{A}$ ) is added in.
4. Trips generated for Edwards area development (Figure B), as calculated by McD, are added in to obtain the 2040 background traffic volumes (Figure 4).
5. The above external trips for ERP were assigned to the roadway system based on the McD trip distribution assumptions (Figure C). This traffic assignment was added to the background traffic (Figure 4) to obtain the total proposed 2040 traffic volumes (Figure 5).

## Conclusions

I. In light of the January 29, 2019 traffic data, an updated evaluation of projected operations at US 6 and I-70 G would be helpful to determine the sensitivity of the roundabout design and to identify the potential need for any improvements to the design.
2. The McD projections for 2040 may be overly conservative. However, using the information and analyses provided in the McD report, I have made adjustments, as described above, to update the projections for the US 6 and I-70 G intersection for design purposes. The resultant proposed 2040 total traffic volumes (included in the attachments) can be forwarded on to MSA for updating the roundabout analysis.



## LEVEL OF SERVICE DEFINITIONS

From Highway Capacity Manual, Transportation Research Board, 2016, 6th Edition
UNSIGNALIZED INTERSECTION LEVEL OF SERVICE (LOS)
Applicable to Two-Way Stop Control, All-Way Stop Control, and Roundabouts

| LOS | Average Vehicle Control Delay | Operational Characteristics |
| :---: | :---: | :---: |
| A | <10 seconds | Normally, vehicles on the stop-controlled approach only have to wait up to 10 seconds before being able to clear the intersection. Left-turning vehicles on the uncontrolled street do not have to wait to make their turn. |
| B | 10 to 15 seconds | Vehicles on the stop-controlled approach will experience delays before being able to clear the intersection. The delay could be up to 15 seconds. Left-turning vehicles on the uncontrolled street may have to wait to make their turn. |
| C | 15 to 25 seconds | Vehicles on the stop-controlled approach can expect delays in the range of 15 to 25 seconds before clearing the intersection. Motorists may begin to take chances due to the long delays, thereby posing a safety risk to through traffic. Left-turning vehicles on the uncontrolled street will now be required to wait to make their turn causing a queue to be created in the turn lane. |
| D | 25 to 35 seconds | This is the point at which a traffic signal may be warranted for this intersection. The delays for the stop-controlled intersection are not considered to be excessive. The length of the queue may begin to block other public and private access points. |
| E | 35 to 50 seconds | The delays for all critical traffic movements are considered to be unacceptable. The length of the queues for the stop-controlled approaches as well as the left-turn movements are extremely long. There is a high probability that this intersection will meet traffic signal warrants. The ability to install a traffic signal is affected by the location of other existing traffic signals. Consideration may be given to restricting the accesses by eliminating the left-turn movements from and to the stop-controlled approach. |
| F | >50 seconds | The delay for the critical traffic movements are probably in excess of 100 seconds. The length of the queues are extremely long. Motorists are selecting alternative routes due to the long delays. The only remedy for these long delays is installing a traffic signal or restricting the accesses. The potential for accidents at this intersection are extremely high due to motorist taking more risky chances. If the median permits, motorists begin making two-stage left-turns. |

## Operational Data

## Main Geometry (ft)

## Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> ? |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 0 | 12.00 | 1 | 14.00 | 1 | 55.00 | 50.00 | 20.00 |
| 2 | West Leg | 90 | 0 | 24.00 | 2 | 25.70 | 2 | 70.00 | 40.00 | 20.00 |
| 3 | South Leg | 160 | 0 | 12.10 | 1 | 24.00 | 2 | 130.00 | 60.00 | 20.00 |
| 4 | East Leg | 265 | 0 | 22.30 | 2 | 24.00 | 2 | 180.00 | 60.00 | 20.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> D | Circulating <br> Width <br> C | Circulating <br> Lanes <br> $\mathbf{n c}$ | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 165.00 | 30.00 | 2 | 24.70 | 2 | 23.30 | 2 |
| 2 | West Leg | 140.00 | 20.00 | 1 | 25.10 | 2 | 24.00 | 2 |
| 3 | South Leg | 165.00 | 30.00 | 2 | 25.00 | 1 | 12.20 | 1 |
| 4 | East Leg | 140.00 | 30.00 | 2 | 24.00 | 2 | 19.40 | 2 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity |  | Entry Calibration |  | Approach Road |  |  | Exit Road |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity + or - | XWalk Factor | Intercept + or - | Slope Factor | V $(\mathrm{ft})$ | Default Capacity | Calib Capacity | $(\mathrm{ft})$ | Default Capacity | Calib Capacity |
| 1 | North Leg | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 23.30 | 3480 | 0 |
| 2 | West Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 3 | South Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 1807 | 0 | 12.20 | 1822 | 0 |
| 4 | East Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3331 | 0 | 19.40 | 2897 | 0 |

2020 AM Peak
50\% Confidence Level
Daylight conditions

Project: West End
Scheme: Existing

## Bypass Geometry

Bypass Approach Geometry (ft)

| Leg | Leg Names | Bypass <br> Type | Bypass <br> Flows | V | nv | Vb | nvb | Vt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | Yield | 235 | 12 | 1 | 12 | 1 | 24 |

Bypass Entry and Exit Geometry (ft)

| Leg | Leg Names | Eb | neb | Lb | Lt | Rb | Phib | Leg | Leg Names | Exit Lanes <br> nex |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | North Leg | 12 | 1 | 20 | 130 | 65.00019 <br> 76 | 30 | 2 | West Leg | 2 |

Bypass Entry Capacity Modifiers and Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity <br> Capacity <br> + or - |  | Cross Walk <br> Factor | Intercept <br> + or - |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 1.000 | 0 | Slope <br> Factor |

2020 AM Peak

Project: West End
Scheme: Existing

Traffic Flow Data (veh/hr)
2020 AM Peak Peak Hour Flows

| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks <br> $\%$ | Flow Modifiers <br> Flow <br> Factor | Peak Hour <br> Factor |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 155 | 250 | 0 | 235 | 2.0 | 1.00 | 0.9 |
| 2 | West Leg | 0 | 335 | 265 | 100 | 0 | 2.0 | 1.00 | 0.9 |
| 3 | South Leg | 0 | 36 | 165 | 160 | 0 | 2.0 | 1.00 | 0.9 |
| 4 | East Leg | 0 | 135 | 145 | 270 | 0 | 2.0 | 1.00 | 0.9 |

## Operational Results

## 2020 AM Peak - 60 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | North Leg | Yield | 405 | 235 | 316 | 316 | 770 | 1064 | 975 | 0.3854 | 0.2438 |
| 2 | West Leg | None | 700 |  | 540 |  | 416 | 1712 |  | 0.4155 |  |
| 3 | South Leg | None | 361 |  | 755 |  | 485 | 1448 |  | 0.2530 |  |
| 4 | East Leg | None | 550 |  | 536 |  | 580 | 1793 |  | 0.3109 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass | Average Delay (sec) |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  | Entry | Bypass |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Leg | Entry | Bypass | Entry | Bypass | Leg |  |  |  |
| 1 | North Leg | Yield | 5.24 | 4.82 | 5.08 | 1.68 | 0.89 | A | A | A |
| 2 | West Leg | None | 6.52 |  | 6.52 | 3.61 |  | A | A |  |
| 3 | South Leg | None | 5.73 |  | 5.73 | 1.64 | A | A |  |  |
| 4 | East Leg | None | 5.48 | 5.48 | 2.36 | A | A |  |  |  |

2020 AM Peak

Project: West End
Scheme: Existing
Rodel-Win1 - Full Geometry

## 2020 AM Peak - 15 minutes

Flows and Capacity

| Leg | Leg Names | Bypass <br> Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit <br> Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | North Leg | Yield | 426 | 247 | 333 | 333 | 810 | 1058 | 970 | 0.4075 | 0.2578 |
| 2 | West Leg | None | 737 |  | 568 |  | 438 | 1682 |  | 0.4443 |  |
| 3 | South Leg | None | 380 |  | 794 |  | 510 | 1421 |  | 0.2707 |  |
| 4 | East Leg | None | 579 |  | 564 |  | 610 | 1772 |  | 0.3306 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | North Leg | Yield | 5.28 | 4.82 | 5.11 | 1.68 | 0.89 | A | A | A |
| 2 | West Leg | None | 6.68 |  | 6.68 | 3.61 |  | A |  | A |
| 3 | South Leg | None | 5.78 |  | 5.78 | 1.64 |  | A |  | A |
| 4 | East Leg | None | 5.52 |  | 5.52 | 2.36 |  | A |  | A |

## Global Results

## Performance and Accidents

## 2020 AM Peak Global Performance

| Parameter | Units | Entries | Bypasses | Total |
| :--- | :---: | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 2016 | 235 | 2251 |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 6017 | 975 | 6992 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 5.84 | 4.82 | 5.73 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| Total Delay | veh.hrs | 3.27 | 0.31 | 3.58 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.7 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 忤 |  |  | 个 | MF |  |
| Traffic Vol, veh/h | 680 | 20 | 25 | 390 | 10 | 20 |
| Future Vol, veh/h | 680 | 20 | 25 | 390 | 10 | 20 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 60 | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 739 | 22 | 27 | 424 | 11 | 22 |


| Major/Minor M | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 761 | 0 | 1228 | 381 |
| Stage 1 | - | - | - | - | 750 | - |
| Stage 2 | - | - | - | - | 478 | - |
| Critical Hdwy | - | - | 4.13 | - | 6.63 | 6.93 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.83 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.43 | - |
| Follow-up Hdwy | - | - | 2.219 | - | 3.519 | 3.319 |
| Pot Cap-1 Maneuver | - | - | 849 | - | 183 | 618 |
| Stage 1 | - | - | - | - | 428 | - |
| Stage 2 | - | - | - | - | 623 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 849 | - | 177 | 618 |
| Mov Cap-2 Maneuver | - | - | - | - | 177 | - |
| Stage 1 | - | - | - | - | 428 | - |
| Stage 2 | - | - | - | - | 603 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.6 |  | 16.8 |  |
| HCM LOS |  |  |  |  | C |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) |  | 338 | - | - | 849 | - |
| HCM Lane V/C Ratio |  | 0.096 | - | - | 0.032 | - |
| HCM Control Delay (s) |  | 16.8 | - | - | 9.4 | - |
| HCM Lane LOS |  | C | - | - | A | - |
| HCM 95th \%tile Q(veh) |  | 0.3 | - | - | 0.1 | - |




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations |  | $\mathbf{7}$ | $\mathbf{1}$ | 体 | 个 |  |
| Traffic Vol, veh/h | 0 | 10 | 20 | 790 | 625 | 10 |
| Future Vol, veh/h | 0 | 10 | 20 | 790 | 625 | 10 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | 0 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 11 | 22 | 859 | 679 | 11 |


|  | Minor2 |  |  |  |  | Major1 |  | Major2 |  |
| :--- | ---: | ---: | ---: | :--- | :--- | :--- | :---: | :---: | :---: |
| Major/Minor |  |  |  |  |  |  |  |  |  |
| Conflicting Flow All | - | 345 | 690 | 0 | - | 0 |  |  |  |
| $\quad$ Stage 1 | - | - | - | - | - | - |  |  |  |
| $\quad$ Stage 2 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy | - | 6.94 | 4.14 | - | - | - |  |  |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |  |  |  |
| Follow-up Hdwy | - | 3.32 | 2.22 | - | - | - |  |  |  |
| Pot Cap-1 Maneuver | 0 | 651 | 900 | - | - | - |  |  |  |
| $\quad$ Stage 1 | 0 | - | - | - | - | - |  |  |  |
| $\quad$ Stage 2 | 0 | - | - | - | - | - |  |  |  |
| Platoon blocked, \% |  |  |  | - | - | - |  |  |  |
| Mov Cap-1 Maneuver | - | 651 | 900 | - | - | - |  |  |  |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |
|  |  |  |  |  |  |  |  |  |  |


| Approach | EB | NB | SB |  |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, s | 10.6 | 0.2 | 0 |  |
| HCM LOS | B |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |
| Capacity (veh/h) | 900 | - | 651 | - |
| HCM Lane V/C Ratio | 0.024 | -0.017 | - | - |
| HCM Control Delay (s) | 9.1 | - | 10.6 | - |
| HCM Lane LOS | A | - | B | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | 0.1 | - |

2020 PM Peak
50\% Confidence Level
Daylight conditions

Project: West End
Scheme: Existing Rodel-Win1 - Full Geometry

## Operational Data

Main Geometry (ft)

## Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> ? |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 0 | 12.00 | 1 | 14.00 | 1 | 55.00 | 50.00 | 20.00 |
| 2 | West Leg | 90 | 0 | 24.00 | 2 | 25.70 | 2 | 70.00 | 40.00 | 20.00 |
| 3 | South Leg | 160 | 0 | 12.10 | 1 | 24.00 | 2 | 130.00 | 60.00 | 20.00 |
| 4 | East Leg | 265 | 0 | 22.30 | 2 | 24.00 | 2 | 180.00 | 60.00 | 20.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> D | Circulating <br> Width <br> C | Circulating <br> Lanes <br> $\mathbf{n c}$ | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 165.00 | 30.00 | 2 | 24.70 | 2 | 23.30 | 2 |
| 2 | West Leg | 140.00 | 20.00 | 1 | 25.10 | 2 | 24.00 | 2 |
| 3 | South Leg | 165.00 | 30.00 | 2 | 25.00 | 1 | 12.20 | 1 |
| 4 | East Leg | 140.00 | 30.00 | 2 | 24.00 | 2 | 19.40 | 2 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity |  | Entry Calibration |  | Approach Road |  |  | Exit Road |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity + or - | XWalk Factor | Intercept + or - | Slope Factor | V $(\mathrm{ft})$ | Default Capacity | Calib Capacity | $(\mathrm{ft})$ | Default Capacity | Calib Capacity |
| 1 | North Leg | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 23.30 | 3480 | 0 |
| 2 | West Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 3 | South Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 1807 | 0 | 12.20 | 1822 | 0 |
| 4 | East Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3331 | 0 | 19.40 | 2897 | 0 |

2020 PM Peak
50\% Confidence Level
Daylight conditions

Project: West End
Scheme: Existing

## Bypass Geometry

Bypass Approach Geometry (ft)

| Leg | Leg Names | Bypass <br> Type | Bypass <br> Flows | V | nv | Vb | nvb | Vt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | Yield | 330 | 12 | 1 | 12 | 1 | 24 |

Bypass Entry and Exit Geometry (ft)

| Leg | Leg Names | Eb | neb | Lb | Lt | Rb | Phib | Leg | Leg Names | Exit Lanes <br> nex | Nmx |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | North Leg | 12 | 1 | 20 | 130 | 65.00020 <br> 384 | 30 | 2 | West Leg | 2 | 2 |

Bypass Entry Capacity Modifiers and Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity <br> Capacity <br> + or - |  | Cross Walk <br> Factor | Intercept <br> + or - |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 1.000 | 0 | Slope <br> Factor |

2020 PM Peak
50\% Confidence Level
Daylight conditions

Project: West End
Scheme: Existing

## Traffic Flow Data (veh/hr)

## 2020 PM Peak Peak Hour Flows

| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks <br> $\%$ | Flow Modifiers <br> Flow <br> Factor | Peak Hour <br> Factor |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 165 | 220 | 0 | 330 | 2.0 | 1.00 | 0.9 |
| 2 | West Leg | 0 | 395 | 395 | 280 | 0 | 2.0 | 1.00 | 0.9 |
| 3 | South Leg | 0 | 23 | 385 | 275 | 0 | 2.0 | 1.00 | 0.9 |
| 4 | East Leg | 0 | 235 | 340 | 165 | 0 | 2.0 | 1.00 | 0.9 |

## Operational Results

## 2020 PM Peak - 60 minutes

Flows and Capacity

| Leg | Leg Names | Bypass | Flows (veh/hr) <br> Type |  |  |  |  | Arrival Flow | Opposing Flow | Exit | Capacity (veh/hr) <br> Cntry |  | Bypass | Entry | Bypass | Flow | Entry | Bypass | Average VCR |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Entry | Bypass |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | North Leg | Yield | 385 | 330 | 598 | 598 | 945 | 960 | 876 | 0.4070 | 0.3827 |  |  |  |  |  |  |  |  |
| 2 | West Leg | None | 1070 |  | 620 |  | 693 | 1628 | 0.6721 |  |  |  |  |  |  |  |  |  |  |
| 3 | South Leg | None | 683 |  | 955 | 735 | 1315 | 0.5309 |  |  |  |  |  |  |  |  |  |  |  |
| 4 | East Leg | None | 740 |  | 803 | 835 | 1594 | 0.4709 |  |  |  |  |  |  |  |  |  |  |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | North Leg | Yield | 5.99 | 6.52 | 6.24 | 1.85 | 1.72 | A | A | A |
| 2 | West Leg | None | 9.49 |  | 9.49 | 8.29 |  | A |  | A |
| 3 | South Leg | None | 9.01 |  | 9.01 | 4.98 |  | A |  | A |
| 4 | East Leg | None | 5.88 |  | 5.88 | 3.51 |  | A |  | A |

2020 PM Peak
50\% Confidence Level
Daylight conditions

Project: West End
Scheme: Existing
Rodel-Win1 - Full Geometry

## 2020 PM Peak - 15 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit <br> Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | North Leg | Yield | 405 | 347 | 629 | 629 | 994 | 948 | 865 | 0.4330 | 0.4073 |
| 2 | West Leg | None | 1126 |  | 652 |  | 729 | 1594 |  | 0.7215 |  |
| 3 | South Leg | None | 719 |  | 1004 |  | 773 | 1282 |  | 0.5720 |  |
| 4 | East Leg | None | 779 |  | 844 |  | 878 | 1564 |  | 0.5046 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass | Average Delay (sec) |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  | Entry | Bypass |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Leg | Entry | Bypass | Entry | Bypass |  |  |  |  |
| 1 | North Leg | Yield | 6.10 | 6.63 | 6.34 | 1.85 | 1.72 | A | A | A |
| 2 | West Leg | None | 10.21 |  | 10.21 | 8.29 |  | B | B |  |
| 3 | South Leg | None | 9.44 |  | 9.44 | 4.98 | A | A |  |  |
| 4 | East Leg | None | 6.09 |  | 6.09 | 3.51 | A | A |  |  |

2020 PM Peak
50\% Confidence Level
Daylight conditions

Project: West End
Scheme: Existing

## Global Results

## Performance and Accidents

## 2020 PM Peak Global Performance

| Parameter | Units | Entries | Bypasses | Total |
| :--- | :---: | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 2878 | 330 | 3208 |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 5497 | 876 | 6373 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 7.98 | 6.52 | 7.83 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| Total Delay | veh.hrs | 6.38 | 0.60 | 6.98 |




| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh | 16.9 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  |  | 「 |  |  | 「 |  | 性 |  |  | 颜 |  |  |
| Traffic Vol，veh／h | 0 | 0 | 20 | 0 | 0 | 475 | 0 | 825 | 125 | 0 | 695 | 5 |  |
| Future Vol，veh／h | 0 | 0 | 20 | 0 | 0 | 475 | 0 | 825 | 125 | 0 | 695 | 5 |  |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |  |
| RT Channelized | － | － | None | － | － | None | － |  | None | － |  | None |  |
| Storage Length | － | － | 0 | － | － | 0 | － | － | － | － | － | － |  |
| Veh in Median Storage，\＃ | \＃ | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |  |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 0 | 0 | 22 | 0 | 0 | 516 | 0 | 897 | 136 | 0 | 755 | 5 |  |



Platoon blocked，\％
Mov Cap－1 Maneuver－－ 618 －-503

Mov Cap－2 Maneuver
Stage 1
Stage 2

| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay，S | 11 | 75.9 | 0 | 0 |
| HCM LOS | B | F |  |  |


| Minor Lane／Major Mvmt | NBT | NBR EBLn1WBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity（veh／h） | - | -618 | 503 | - | - |
| HCM Lane V／C Ratio | - | -0.035 | 1.026 | - | - |
| HCM Control Delay（s） | - | - | 11 | 75.9 | - |
| HCM Lane LOS | - | - | B | F | - |
| HCM 95th \％tile Q（veh） | - | - | 0.1 | 14.8 | - |

## Notes

$\sim$ ：Volume exceeds capacity $\$$ ：Delay exceeds $300 s \quad+$ ：Computation Not Defined $\quad$ ：All major volume in platoon

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


|  | Major2 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Major/Minor | Minor2 | Major1 |  |  |  |
| Conflicting Flow All | - | 312 | 623 | 0 | - |
| $\quad$ Stage 1 | - | - | - | - | - |
| $\quad$ Stage 2 | - | - | - | - | - |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 12.1 | 0.6 | 0 |
| HCM LOS | B |  |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 954 | -684 | - | - |
| HCM Lane V/C Ratio | 0.1 | -0.264 | - | - |
| HCM Control Delay (s) | 9.2 | -12.1 | - | - |
| HCM Lane LOS | A | - | $B$ | - |
| HCM 95th \%tile Q(veh) | 0.3 | - | 1.1 | - |
| (ven | - |  |  |  |

## Operational Data

## Main Geometry (ft)

## Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> ? |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 0 | 12.00 | 1 | 14.00 | 1 | 55.00 | 50.00 | 20.00 |
| 2 | West Leg | 90 | 0 | 24.00 | 2 | 25.70 | 2 | 70.00 | 40.00 | 20.00 |
| 3 | South Leg | 160 | 0 | 12.10 | 1 | 24.00 | 2 | 130.00 | 60.00 | 20.00 |
| 4 | East Leg | 265 | 0 | 22.30 | 2 | 24.00 | 2 | 180.00 | 60.00 | 20.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> D | Circulating <br> Width <br> C | Circulating <br> Lanes <br> $\mathbf{n c}$ | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 165.00 | 30.00 | 2 | 24.70 | 2 | 23.30 | 2 |
| 2 | West Leg | 140.00 | 20.00 | 1 | 25.10 | 2 | 24.00 | 2 |
| 3 | South Leg | 165.00 | 30.00 | 2 | 25.00 | 1 | 12.20 | 1 |
| 4 | East Leg | 140.00 | 30.00 | 2 | 24.00 | 2 | 19.40 | 2 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity |  | Entry Calibration |  | Approach Road |  |  | Exit Road |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity + or - | XWalk Factor | Intercept + or - | Slope Factor | V $(\mathrm{ft})$ | Default Capacity | Calib Capacity | $(\mathrm{ft})$ | Default Capacity | Calib Capacity |
| 1 | North Leg | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 23.30 | 3480 | 0 |
| 2 | West Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 3 | South Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 1807 | 0 | 12.20 | 1822 | 0 |
| 4 | East Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3331 | 0 | 19.40 | 2897 | 0 |

## Bypass Geometry

Bypass Approach Geometry (ft)

| Leg | Leg Names | Bypass <br> Type | Bypass <br> Flows | V | nv | Vb | nvb | Vt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | Yield | 345 | 12 | 1 | 12 | 1 | 24 |

Bypass Entry and Exit Geometry (ft)

| Leg | Leg Names | Eb | neb | Lb | Lt | Rb | Phib | Leg | Leg Names | Exit Lanes <br> nex |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | North Leg | 12 | 1 | 20 | 130 | 65.00019 <br> 76 | 30 | 2 | West Leg | 2 |

Bypass Entry Capacity Modifiers and Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity <br> Capacity <br> + or - |  | Cross Walk <br> Factor | Intercept <br> + or - |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 1.000 | 0 | Slope <br> Factor |

## Traffic Flow Data (veh/hr)

## 2025 AM Peak Peak Hour Flows

| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks <br> $\%$ | Flow Modifiers <br> Flow <br> Factor | Peak Hour <br> Factor |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 159 | 256 | 0 | 345 | 2.0 | 1.00 | 0.9 |
| 2 | West Leg | 0 | 418 | 322 | 123 | 0 | 2.0 | 1.00 | 0.9 |
| 3 | South Leg | 0 | 67 | 169 | 164 | 0 | 2.0 | 1.00 | 0.9 |
| 4 | East Leg | 0 | 138 | 214 | 277 | 0 | 2.0 | 1.00 | 0.9 |

## Operational Results

## 2025 AM Peak - 60 minutes

Flows and Capacity

| Leg | Leg Names | Bypass | Flows (veh/hr) <br> Type |  |  |  |  | Arrival Flow | Opposing Flow | Exit | Capacity (veh/hr) <br> Cntry |  | Bypass | Entry | Bypass | Flow | Entry | Bypass | Average VCR |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Entry | Bypass |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | North Leg | Yield | 415 | 345 | 419 | 419 | 864 | 1026 | 939 | 0.4100 | 0.3727 |  |  |  |  |  |  |  |  |
| 2 | West Leg | None | 863 |  | 553 |  | 626 | 1698 | 0.5179 |  |  |  |  |  |  |  |  |  |  |
| 3 | South Leg | None | 400 |  | 899 | 517 | 1352 | 0.3005 |  |  |  |  |  |  |  |  |  |  |  |
| 4 | East Leg | None | 629 |  | 654 | 645 | 1705 | 0.3741 |  |  |  |  |  |  |  |  |  |  |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | North Leg | Yield | 5.64 | 6.00 | 5.80 | 1.86 | 1.64 | A | A | A |
| 2 | West Leg | None | 7.93 |  | 7.93 | 5.42 |  | A |  | A |
| 3 | South Leg | None | 6.17 |  | 6.17 | 1.97 |  | A |  | A |
| 4 | East Leg | None | 5.73 |  | 5.73 | 2.85 |  | A |  | A |

## 2025 AM Peak - 15 minutes

Flows and Capacity

| Leg | Leg Names | Bypass <br> Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit <br> Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | North Leg | Yield | 437 | 363 | 441 | 441 | 909 | 1018 | 931 | 0.4344 | 0.3950 |
| 2 | West Leg | None | 908 |  | 582 |  | 659 | 1668 |  | 0.5542 |  |
| 3 | South Leg | None | 421 |  | 946 |  | 544 | 1321 |  | 0.3231 |  |
| 4 | East Leg | None | 662 |  | 688 |  | 679 | 1680 |  | 0.3991 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass | Average Delay (sec) |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  | Entry | Bypass |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Leg | Entry | Bypass | Entry | Bypass |  |  |  |  |
| 1 | North Leg | Yield | 5.71 | 6.06 | 5.87 | 1.86 | 1.64 | A | A | A |
| 2 | West Leg | None | 8.22 |  | 8.22 | 5.42 |  | A | A |  |
| 3 | South Leg | None | 6.28 |  | 6.28 | 1.97 |  | A |  |  |
| 4 | East Leg | None | 5.83 |  | 5.83 | 2.85 | A | A |  |  |

## Global Results

## Performance and Accidents

## 2025 AM Peak Global Performance

| Parameter | Units | Entries | Bypasses | Total |
| :--- | :---: | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 2307 | 345 | 2652 |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 5781 | 939 | 6720 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 6.61 | 6.00 | 6.53 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| Total Delay | veh.hrs | 4.24 | 0.57 | 4.81 |



| Major/Minor | Major1 | Major2 |  |  | Minor1 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| Conflicting Flow All | 0 | 0 | 940 | 0 | 1635 | 470 |  |
| $\quad$ Stage 1 | - | - | - | - | 929 | - |  |
| $\quad$ Stage 2 | - | - | - | - | 706 | - |  |
| Critical Hdwy | - | - | 4.13 | - | 6.63 | 6.93 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.83 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.43 | - |  |
| Follow-up Hdwy | - | - | 2.219 | -3.519 | 3.319 |  |  |
| Pot Cap-1 Maneuver | - | - | 727 | - | 101 | 541 |  |
| $\quad$ Stage 1 | - | - | - | - | 346 | - |  |
| Stage 2 | - | - | - | - | 488 | - |  |
| Platoon blocked, \% | - | - |  | - |  |  |  |
| Mov Cap-1 Maneuver | - | - | 727 | - | 97 | 541 |  |
| Mov Cap-2 Maneuver | - | - | - | - | 97 | - |  |
| Stage 1 | - | - | - | - | 346 | - |  |
| Stage 2 | - | - | - | - | 470 | - |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0.4 | 24.8 |
| HCM LOS |  |  | C |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 214 | - | - | 727 | - |
| HCM Lane V/C Ratio | 0.152 | - | -0.037 | - |  |
| HCM Control Delay (s) | 24.8 | - | - | 10.1 | - |
| HCM Lane LOS | C | - | - | B | - |
| HCM 95th \%tile Q(veh) | 0.5 | - | - | 0.1 | - |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.6 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  |  | F |  |  | F |  | 个 ${ }^{\text {a }}$ |  |  | 性 |  |  |
| Traffic Vol, veh/h | 0 | 0 | 10 | 0 | 0 | 65 | 0 | 840 | 25 | 0 | 750 | 5 |  |
| Future Vol, veh/h | 0 | 0 | 10 | 0 | 0 | 65 | 0 | 840 | 25 | 0 | 750 | 5 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |  |
| Storage Length | - | - | 0 | - | - | 0 | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | , | 2 | 2 |  |
| Mvmt Flow | 0 | 0 | 11 | 0 | 0 | 71 | 0 | 913 | 27 | 0 | 815 | 5 |  |



Platoon blocked, \%

| Mov Cap-1 Maneuver | - | - | 591 | - | - | 540 | - | - | - | - | - | - |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - | - | - | - | - | - | - |

Stage 2

| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, s | 11.2 | 12.7 | 0 | 0 |


| Minor Lane/Major Mvmt | NBT | NBR EBLn1WBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | - | -591 | 540 | - | - |
| HCM Lane V/C Ratio | - | -0.018 | 0.131 | - | - |
| HCM Control Delay (s) | - | - | 11.2 | 12.7 | - |
| HCM Lane LOS | - | - | - |  |  |
| HCM 95th \%tile Q(veh) | - | - | 0.1 | 0.4 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |


| Major/Minor | Minor2 |  | Major1 | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 411 | 821 | 0 | - | 0 |  |
| Stage 1 | - |  | - | - | - | - |  |
| Stage 2 | - |  | - | - | - | - |  |
| Critical Hdwy | - | 6.94 | 4.14 | - | - | - |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |  |
| Follow-up Hdwy | - | 3.32 | 2.22 | - | - | - |  |
| Pot Cap-1 Maneuver | 0 | 590 | 804 | - | - | - |  |
| Stage 1 | 0 | - | - | - | - | - |  |
| Stage 2 | 0 | - | - | - | - | - |  |
| Platoon blocked, \% |  |  |  | - | - | - |  |
| Mov Cap-1 Maneuver | - | 590 | 804 | - | - | - |  |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |  |
| Stage 1 | - | - | - | - | - | - |  |
| Stage 2 | - | - | - | - | - | - |  |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 11.2 | 0.2 | 0 |
| HCM LOS | B |  |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 804 | -590 | - | - |
| HCM Lane V/C Ratio | 0.027 | -0.018 | - | - |
| HCM Control Delay (s) | 9.6 | -11.2 | - | - |
| HCM Lane LOS | A | - | $B$ | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | 0.1 | - |
| (ven |  |  |  |  |

## Operational Data

## Main Geometry (ft)

## Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> ? |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 0 | 12.00 | 1 | 14.00 | 1 | 55.00 | 50.00 | 20.00 |
| 2 | West Leg | 90 | 0 | 24.00 | 2 | 25.70 | 2 | 70.00 | 40.00 | 20.00 |
| 3 | South Leg | 160 | 0 | 12.10 | 1 | 24.00 | 2 | 130.00 | 60.00 | 20.00 |
| 4 | East Leg | 265 | 0 | 22.30 | 2 | 24.00 | 2 | 180.00 | 60.00 | 20.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> D | Circulating <br> Width <br> C | Circulating <br> Lanes <br> $\mathbf{n c}$ | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 165.00 | 30.00 | 2 | 24.70 | 2 | 23.30 | 2 |
| 2 | West Leg | 140.00 | 20.00 | 1 | 25.10 | 2 | 24.00 | 2 |
| 3 | South Leg | 165.00 | 30.00 | 2 | 25.00 | 1 | 12.20 | 1 |
| 4 | East Leg | 140.00 | 30.00 | 2 | 24.00 | 2 | 19.40 | 2 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity |  | Entry Calibration |  | Approach Road |  |  | Exit Road |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity + or - | XWalk Factor | Intercept + or - | Slope Factor | V $(\mathrm{ft})$ | Default Capacity | Calib Capacity | $(\mathrm{ft})$ | Default Capacity | Calib Capacity |
| 1 | North Leg | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 23.30 | 3480 | 0 |
| 2 | West Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 3 | South Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 1807 | 0 | 12.20 | 1822 | 0 |
| 4 | East Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3331 | 0 | 19.40 | 2897 | 0 |

## Bypass Geometry

Bypass Approach Geometry (ft)

| Leg | Leg Names | Bypass <br> Type | Bypass <br> Flows | V | nv | Vb | nvb | Vt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | Yield | 548 | 12 | 1 | 12 | 1 | 24 |

Bypass Entry and Exit Geometry (ft)

| Leg | Leg Names | Eb | neb | Lb | Lt | Rb | Phib | Leg | Leg Names | Exit Lanes <br> nex | Nmx |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | North Leg | 12 | 1 | 20 | 130 | 65.00020 <br> 384 | 30 | 2 | West Leg | 2 | 2 |

Bypass Entry Capacity Modifiers and Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity <br> Capacity <br> + or - |  | Cross Walk <br> Factor | Intercept <br> + or - |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 1.000 | 0 | Slope <br> Factor |

## Traffic Flow Data (veh/hr)

2025 PM Peak Peak Hour Flows

| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks <br> $\%$ | Flow Modifiers <br> Flow <br> Factor | Peak Hour <br> Factor |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 169 | 225 | 0 | 548 | 2.0 | 1.00 | 0.9 |
| 2 | West Leg | 0 | 545 | 495 | 322 | 0 | 2.0 | 1.00 | 0.9 |
| 3 | South Leg | 0 | 79 | 405 | 282 | 0 | 2.0 | 1.00 | 0.9 |
| 4 | East Leg | 0 | 241 | 479 | 169 | 0 | 2.0 | 1.00 | 0.9 |

## Operational Results

## 2025 PM Peak - 60 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | North Leg | Yield | 394 | 548 | 799 | 799 | 1117 | 885 | 805 | 0.4525 | 0.7019 |
| 2 | West Leg | None | 1362 |  | 635 |  | 1105 | 1613 |  | 0.8834 |  |
| 3 | South Leg | None | 766 |  | 1207 |  | 787 | 1147 |  | 0.6894 |  |
| 4 | East Leg | None | 889 |  | 1027 |  | 945 | 1427 |  | 0.6358 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | North Leg | Yield | 6.98 | 13.66 | 10.86 | 2.23 | 6.26 | A | B | B |
| 2 | West Leg | None | 20.28 |  | 20.28 | 23.24 |  | C |  | C |
| 3 | South Leg | None | 13.78 |  | 13.78 | 8.84 |  | B |  | B |
| 4 | East Leg | None | 8.58 |  | 8.58 | 6.34 |  | A |  | A |

## 2025 PM Peak - 15 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | North Leg | Yield | 415 | 577 | 839 | 839 | 1168 | 871 | 791 | 0.4837 | 0.7512 |
| 2 | West Leg | None | 1434 |  | 667 |  | 1160 | 1579 |  | 0.9497 |  |
| 3 | South Leg | None | 806 |  | 1259 |  | 824 | 1112 |  | 0.7471 |  |
| 4 | East Leg | None | 936 |  | 1074 |  | 988 | 1393 |  | 0.6846 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | North Leg | Yield | 7.17 | 14.66 | 11.53 | 2.23 | 6.26 | A | B | B |
| 2 | West Leg | None | 23.24 |  | 23.24 | 23.24 |  | C |  | C |
| 3 | South Leg | None | 14.92 |  | 14.92 | 8.84 |  | B |  | B |
| 4 | East Leg | None | 9.18 |  | 9.18 | 6.34 |  | A |  | A |

## Global Results

## Performance and Accidents

## 2025 PM Peak Global Performance

| Parameter | Units | Entries | Bypasses | Total |
| :--- | :---: | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 3411 | 548 | 3959 |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 5073 | 805 | 5878 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 14.23 | 13.66 | 14.15 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | B | B | B |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | B | B | B |
| Total Delay | veh.hrs | 13.49 | 2.08 | 15.57 |



| Major/Minor | Major1 | Major2 |  |  | Minor1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 0 | 0 | 1424 | 0 | 2706 | 712 |
| $\quad$ Stage 1 | - | - | - | - | 1413 | - |
| $\quad$ Stage 2 | - | - | - | - | 1293 | - |
| Critical Hdwy | - | - | 4.13 | - | 6.63 | 6.93 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.83 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.43 | - |
| Follow-up Hdwy | - | - | 2.219 | - | 3.519 | 3.319 |
| Pot Cap-1 Maneuver | - | - | 476 | - | $\sim 20$ | 376 |
| $\quad$ Stage 1 | - | - | - | - | 191 | - |
| $\quad$ Stage 2 | - | - | - | - | 256 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 476 | - | $\sim 16$ | 376 |
| Mov Cap-2 Maneuver | - | - | - | - | $\sim 16$ | - |
| $\quad$ Stage 1 | - | - | - | - | 191 | - |
| Stage 2 | - | - | - | - | 207 | - |
|  |  |  |  |  |  |  |


| Approach | EB | WB | NB |
| :--- | ---: | :---: | ---: |
| HCM Control Delay, s | 0 | 1.1 | $\$ 1588.1$ |
| HCM LOS |  | F |  |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 34 | - | - | 476 | - |
| HCM Lane V/C Ratio | 3.996 | - | -0.194 | - |  |
| HCM Control Delay (s) | $\$ 1588.1$ | - | - | 14.4 | - |
| HCM Lane LOS | F | - | - | B | - |
| HCM 95th \%tile Q(veh) | 15.9 | - | - | 0.7 | - |

[^2]| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh | 24.9 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | 「゙ |  |  | 「゙ |  | 中 ${ }^{\text {a }}$ |  |  | 中 ${ }^{\text {a }}$ |  |
| Traffic Vol，veh／h | 0 | 0 | 20 | 0 | 0 | 475 | 0 | 1000 | 125 | 0 | 920 | 5 |
| Future Vol，veh／h | 0 | 0 | 20 | 0 | 0 | 475 | 0 | 1000 | 125 | 0 | 920 | 5 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | － | － | None | － | － | None | － | － | None | － | － | None |
| Storage Length | － | － | 0 | － | － | 0 | － | － | － | － | － | － |
| Veh in Median Storage，\＃ | \＃ | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 22 | 0 | 0 | 516 | 0 | 1087 | 136 | 0 | 1000 | 5 |



Platoon blocked，\％
Mov Cap－1 Maneuver－ 514 －$-\sim 436$

Mov Cap－2 Maneuver
Stage 1
Stage 2

| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay，s | 12.3 | 132.9 | 0 | 0 |
| HCM LOS | B | F |  |  |


| Minor Lane／Major Mvmt | NBT | NBR EBLn1WBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity（veh／h） | - | -514 | 436 | - | - |
| HCM Lane V／C Ratio | - | -0.042 | 1.184 | - | - |
| HCM Control Delay（s） | - | - | 12.3 | 132.9 | - |
| HCM Lane LOS | - | - | - | F | - |
| HCM 95th \％tile Q（veh） | - | - | 0.1 | 19.8 | - |

## Notes

$\sim$ ：Volume exceeds capacity $\$$ ：Delay exceeds $300 \mathrm{~s} \quad+$ ：Computation Not Defined＊：All major volume in platoon


| Major/Minor | Minor2 |  | Major1 | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 441 | 881 | 0 | - | 0 |  |
| Stage 1 | - |  | - | - | - | - |  |
| Stage 2 | - |  | - | - | - | - |  |
| Critical Hdwy | - | 6.94 | 4.14 | - | - | - |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |  |
| Follow-up Hdwy | - | 3.32 | 2.22 | - | - | - |  |
| Pot Cap-1 Maneuver | 0 | 564 | 763 | - | - | - |  |
| Stage 1 | 0 | - | - | - | - | - |  |
| Stage 2 | 0 | - | - | - | - | - |  |
| Platoon blocked, \% |  |  |  | - | - | - |  |
| Mov Cap-1 Maneuver | - | 564 | 763 | - | - | - |  |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |  |
| Stage 1 | - | - | - | - | - | - |  |
| Stage 2 | - | - | - | - | - | - |  |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 14.5 | 0.6 | 0 |
| HCM LOS | B |  |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |
| :--- | ---: | ---: | ---: | :---: |
| Capacity (veh/h) | 763 | -564 | - | - |
| HCM Lane V/C Ratio | 0.128 | -0.328 | - | - |
| HCM Control Delay (s) | 10.4 | -14.5 | - | - |
| HCM Lane LOS | B | - | $B$ | - |
| HCM 95th \%tile Q(veh) | 0.4 | - | 1.4 | - |

## Scheme Summary

## Control Data

Control Data and Model Parameters

| West End | 2025 PHF Flow Profile (veh) |
| :--- | :--- |
| 2025 Total Traffic | 7.5 min Time Slice |
| Rodel-Win1 | Queuing Delays (sec) |
| Right Hand Drive | Daylight conditions |
| AM Peak Hour | Peak 60/15 min Results |
| Full Geometry | Output flows: Vehicles |
| English Units (ft) | $50 \%$ Confidence Level |

## Operational Data

## Main Geometry (ft)

## Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> $\boldsymbol{\Phi}$ |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 0 | 12.00 | 1 | 14.00 | 1 | 55.00 | 50.00 | 20.00 |
| 2 | West Leg | 90 | 0 | 24.00 | 2 | 25.70 | 2 | 70.00 | 40.00 | 20.00 |
| 3 | South Leg | 160 | 0 | 12.10 | 1 | 24.00 | 2 | 130.00 | 60.00 | 20.00 |
| 4 | East Leg | 265 | 0 | 22.30 | 2 | 24.00 | 2 | 180.00 | 60.00 | 20.00 |

## Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> $\mathbf{D}$ | Circulating <br> Width <br> $\mathbf{C}$ | Circulating <br> Lanes <br> $\mathbf{n c}$ | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 165.00 | 30.00 | 2 | 24.70 | 2 | 23.30 | 2 |
| 2 | West Leg | 140.00 | 20.00 | 1 | 25.10 | 2 | 24.00 | 2 |
| 3 | South Leg | 165.00 | 30.00 | 2 | 25.00 | 1 | 12.20 | 1 |
| 4 | East Leg | 140.00 | 30.00 | 2 | 24.00 | 2 | 19.40 | 2 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity <br> Capacity <br> + or - |  | XWalk <br> Factor | Entry Calibration <br> Intercept <br> + or - |  | Slope <br> Factor | Approach Road   <br> (ft)   | Default <br> Capacity | Calib <br> Capacity | V <br> (ft) |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | North Leg | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 23.30 | Default <br> Capacity | Calib <br> Capacity |
| 2 | West Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 3 | South Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 1807 | 0 | 12.20 | 1822 | 0 |
| 4 | East Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3331 | 0 | 19.40 | 2897 | 0 |

## Bypass Geometry

Bypass Approach Geometry (ft)

| Leg | Leg Names | Bypass <br> Type | Bypass <br> Flows | $\mathbf{V}$ | nv | Vb | nvb | Vt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | Yield | 345 | 12 | 1 | 12 | 1 | 24 |

Bypass Entry and Exit Geometry (ft)

| Leg | Leg Names | Eb | neb | Lb | Lt | Rb | Phib | Leg | Leg Names |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | North Leg | 12 | 1 | 20 | 130 | 65.00017 <br> 888 | 30 | 2 | West Leg |
| nex |  | 2 | 2 |  |  |  |  |  |  |

## Bypass Entry Capacity Modifiers and Calibration (veh/hr)

| Leg | Leg Names | Capacity <br> + or - | Entry Capacity <br> Cross Walk <br> Factor | Intercept <br> + or - | Calibration <br> Factor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 1.000 | 0 | 1.000 |

## Traffic Flow Data (veh/hr)

## 2025 AM Peak Peak Hour Flows

| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks <br> $\%$ | Flow Modifiers <br> Flow <br> Factor | Peak Hour <br> Factor |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 49 | 193 | 272 | 0 | 345 | 2.0 | 1.00 | 0.9 |
| 2 | West Leg | 21 | 413 | 322 | 123 | 0 | 2.0 | 1.00 | 0.9 |
| 3 | South Leg | 0 | 82 | 165 | 164 | 0 | 2.0 | 1.00 | 0.9 |
| 4 | East Leg | 0 | 138 | 232 | 277 | 0 | 2.0 | 1.00 | 0.9 |

## Operational Results

## 2025 AM Peak - 60 minutes

## Delays, Queues and Level of Service

| Leg | Leg Names | Bypass | Average Delay (sec) |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  | Entry | Bypass |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Leg | Entry | Bypass | Entry | Bypass | Leg |  |  |  |
| 1 | North Leg | Yield | 6.94 | 6.19 | 6.64 | 2.86 | 1.70 | A | A | A |
| 2 | West Leg | None | 9.37 |  | 9.37 | 6.58 |  | A | A |  |
| 3 | South Leg | None | 6.56 |  | 6.56 | 2.17 |  | A |  |  |
| 4 | East Leg | None | 6.01 |  | 6.01 | 3.09 | A | A |  |  |

## 2025 AM Peak - 15 minutes

## Delays, Queues and Level of Service

| Leg | Leg Names | Bypass | Average Delay (sec) |  |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  | Entry |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |  |  |
| 1 | North Leg | Yield | 7.12 | 6.27 | 6.78 | 2.86 | 1.70 | A | A | A |
| 2 | West Leg | None | 9.84 |  | 9.84 | 6.58 |  | A | A |  |
| 3 | South Leg | None | 6.72 |  | 6.72 | 2.17 |  | A |  |  |
| 4 | East Leg | None | 6.14 |  | 6.14 | 3.09 | A | A |  |  |

## Global Results

## Performance and Accidents

## 2025 AM Peak Global Performance

| Parameter | Units | Entries | Bypasses | Total |
| :--- | :---: | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 2451 | 345 | 2796 |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 5536 | 920 | 6456 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 7.50 | 6.19 | 7.34 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | A | A | A |
| Total Delay | veh.hrs | 5.11 | 0.59 | 5.70 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.7 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 个 | $\mathbf{7}$ |  | 4 | Mr |  |
| Traffic Vol, veh/h | 861 | 20 | 25 | 629 | 10 | 20 |
| Future Vol, veh/h | 861 | 20 | 25 | 629 | 10 | 20 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 140 | 60 | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 936 | 22 | 27 | 684 | 11 | 22 |


| Major/Minor M | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 958 | 0 | 1674 | 936 |
| Stage 1 | - | - | - | - | 936 | - |
| Stage 2 | - | - | - | - | 738 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 718 | - | 105 | 321 |
| Stage 1 | - | - | - | - | 382 | - |
| Stage 2 | - | - | - | - | 473 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 718 | - | 101 | 321 |
| Mov Cap-2 Maneuver | - | - | - | - | 101 | - |
| Stage 1 | - | - | - | - | 382 | - |
| Stage 2 | - | - | - | - | 455 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.4 |  | 28.4 |  |
| HCM LOS |  |  |  |  | D |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) |  | 186 | - | - | 718 | - |
| HCM Lane V/C Ratio |  | 0.175 | - | - | 0.038 | - |
| HCM Control Delay (s) |  | 28.4 | - | - | 10.2 | - |
| HCM Lane LOS |  | D | - | - | B | - |
| HCM 95th \%tile Q(veh) |  | 0.6 | - | - | 0.1 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay，s／veh | 0.3 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 个中 | 体 | $\mathbf{F}$ |  | $\mathbf{7}$ |
| Traffic Vol，veh／h | 0 | 881 | 615 | 64 | 0 | 39 |
| Future Vol，veh／h | 0 | 881 | 615 | 64 | 0 | 39 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | 0 | - | 0 |
| Veh in Median Storage，\＃ | - | 0 | 0 | - | 0 | - |
| Grade，\％ | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles，$\%$ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 958 | 668 | 70 | 0 | 42 |





Platoon blocked, \%

| Mov Cap-1 Maneuver | - | - | 581 | - | - | 522 | - | - | - | - | - | - |
| :---: | :---: | :---: | ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - | - | - | - | - | - | - |

Stage 2

| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | :---: | :---: |
| HCM Control Delay, s | 13 | 13 | 0 | 0 |
| HCM LOS | B | B |  |  |


| Minor Lane/Major Mvmt | NBT | NBR EBLn1WBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | - | -581 | 522 | - | - |
| HCM Lane V/C Ratio | - | -0.223 | 0.135 | - | - |
| HCM Control Delay (s) | - | - | 13 | 13 | - |



| Major/Minor | Minor2 |  |  |  |  |  | Major1 | Major2 |
| :--- | ---: | ---: | ---: | ---: | :--- | :---: | :---: | :---: |
| Conflicting Flow All | - | 422 | 843 | 0 | - |  |  |  |
| $\quad$ Stage 1 | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - |  |  |  |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 11.3 | 0.2 | 0 |
| HCM LOS | B |  |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |
| :--- | ---: | ---: | ---: | :---: |
| Capacity (veh/h) | 789 | -580 | - | - |
| HCM Lane V/C Ratio | 0.028 | -0.019 | - | - |
| HCM Control Delay (s) | 9.7 | -11.3 | - | - |
| HCM Lane LOS | A | - | B | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | 0.1 | - |
| (ven |  |  |  |  |

## Scheme Summary

## Control Data

Control Data and Model Parameters

| West End | 2025 PHF Flow Profile (veh) |
| :--- | :--- |
| 2025 Total Traffic | 7.5 min Time Slice |
| Rodel-Win1 | Queuing Delays (sec) |
| Right Hand Drive | Daylight conditions |
| PM Peak Hour | Peak 60/15 min Results |
| Full Geometry | Output flows: Vehicles |
| English Units (ft) | $50 \%$ Confidence Level |

## Operational Data

## Main Geometry (ft)

## Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> $\boldsymbol{\Phi}$ |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 0 | 12.00 | 1 | 14.00 | 1 | 55.00 | 50.00 | 20.00 |
| 2 | West Leg | 90 | 0 | 24.00 | 2 | 25.70 | 2 | 70.00 | 40.00 | 20.00 |
| 3 | South Leg | 160 | 0 | 12.10 | 1 | 24.00 | 2 | 130.00 | 60.00 | 20.00 |
| 4 | East Leg | 265 | 0 | 22.30 | 2 | 24.00 | 2 | 180.00 | 60.00 | 20.00 |

## Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> $\mathbf{D}$ | Circulating <br> Width <br> $\mathbf{C}$ | Circulating <br> Lanes <br> $\mathbf{n c}$ | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 165.00 | 30.00 | 2 | 24.70 | 2 | 23.30 | 2 |
| 2 | West Leg | 140.00 | 20.00 | 1 | 25.10 | 2 | 24.00 | 2 |
| 3 | South Leg | 165.00 | 30.00 | 2 | 25.00 | 1 | 12.20 | 1 |
| 4 | East Leg | 140.00 | 30.00 | 2 | 24.00 | 2 | 19.40 | 2 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | $\begin{array}{c}\text { Entry Capacity } \\ \text { Capacity } \\ \text { + or }-\end{array}$ |  | $\begin{array}{c}\text { XWalk } \\ \text { Factor }\end{array}$ | $\begin{array}{c}\text { Entry Calibration } \\ \text { Intercept } \\ \text { +or }-\end{array}$ | $\begin{array}{c}\text { Slope } \\ \text { Factor }\end{array}$ |  |  | $\begin{array}{c}\text { Approach Road } \\ \text { (ft) }\end{array}$ | $\begin{array}{c}\text { Default } \\ \text { Capacity }\end{array}$ | $\begin{array}{c}\text { Calib } \\ \text { Capacity }\end{array}$ |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | North Leg | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 23.30 | $\begin{array}{c}\text { Exit Road } \\ \text { (ft) }\end{array}$ | $\begin{array}{c}\text { Default } \\ \text { Capacity }\end{array}$ |
| Capacity |  |  |  |  |  |  |  |  |  |  |  |$)$

## Bypass Geometry

Bypass Approach Geometry (ft)

| Leg | Leg Names | Bypass <br> Type | Bypass <br> Flows | $\mathbf{V}$ | nv | Vb | nvb | Vt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | Yield | 548 | 12 | 1 | 12 | 1 | 24 |

Bypass Entry and Exit Geometry (ft)

| Leg | Leg Names | Entry Geometry |  |  |  |  |  | Leg | Leg Names | Exit Lanes |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Eb | neb | Lb | Lt | Rb | Phib |  |  | nex | Nmx |
| 1 | North Leg | 12 | 1 | 20 | 130 | $\begin{gathered} 65.00019 \\ 136 \end{gathered}$ | 30 | 2 | West Leg | 2 | 2 |

## Bypass Entry Capacity Modifiers and Calibration (veh/hr)

| Leg | Leg Names | Capacity <br> + or - | Entry Capacity <br> Cross Walk <br> Factor | Intercept <br> + or - | Calibration <br> Sactor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 1.000 | 0 | 1.000 |

## Traffic Flow Data (veh/hr)

## 2025 PM Peak Peak Hour Flows

| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks <br> $\%$ | Flow Modifiers <br> Flow <br> Factor | Peak Hour <br> Factor |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 40 | 197 | 238 | 0 | 548 | 2.0 | 1.00 | 0.9 |
| 2 | West Leg | 30 | 542 | 495 | 322 | 0 | 2.0 | 1.00 | 0.9 |
| 3 | South Leg | 0 | 96 | 402 | 282 | 0 | 2.0 | 1.00 | 0.9 |
| 4 | East Leg | 0 | 241 | 508 | 169 | 0 | 2.0 | 1.00 | 0.9 |

## Operational Results

## 2025 PM Peak - 60 minutes

## Delays, Queues and Level of Service

| Leg | Leg Names | Bypass | Average Delay (sec) |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  | Entry | Bypass |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Leg | Entry | Bypass | Entry | Bypass | Leg |  |  |  |
| 1 | North Leg | Yield | 8.87 | 15.19 | 12.25 | 3.46 | 7.03 | A | C | B |
| 2 | West Leg | None | 32.54 |  | 32.54 | 39.55 |  | D | D |  |
| 3 | South Leg | None | 16.70 |  | 16.70 | 10.88 |  | C |  |  |
| 4 | East Leg | None | 10.02 |  | 10.02 | 7.70 | C | B |  |  |

## 2025 PM Peak-15 minutes

## Delays, Queues and Level of Service

| Leg | Leg Names | Bypass | Average Delay (sec) |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  | Entry | Bypass |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Leg | Entry | Bypass | Entry | Bypass | Leg |  |  |  |
| 1 | North Leg | Yield | 9.26 | 16.45 | 13.11 | 3.46 | 7.03 | A | C | B |
| 2 | West Leg | None | 37.94 |  | 37.94 | 39.55 |  | E | E |  |
| 3 | South Leg | None | 18.08 |  | 18.08 | 10.88 |  | C |  |  |
| 4 | East Leg | None | 10.82 |  | 10.82 | 7.70 | C | B |  |  |

## Global Results

## Performance and Accidents

## 2025 PM Peak Global Performance

| Parameter | Units | Entries | Bypasses | Total |
| :--- | :---: | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 3562 | 548 | 4110 |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 4840 | 779 | 5619 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 20.11 | 15.19 | 19.45 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | C | B | B |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | C | C | C |
| Total Delay | veh.hrs | 19.90 | 2.31 | 22.21 |



| Major/Minor | Major1 | Major2 |  | Minor1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 1454 | 0 | 2753 | 1432 |
| Stage 1 | - |  |  |  | 1432 |  |
| Stage 2 | - | - |  |  | 1321 |  |
| Critical Hdwy |  |  | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - |  |  | 5.42 |  |
| Critical Hdwy Stg 2 |  |  |  |  | 5.42 |  |
| Follow-up Hdwy |  |  | 2.218 |  | 3.518 | 3.318 |
| Pot Cap-1 Maneuver |  | - | 465 |  | ~22 | 165 |
| Stage 1 | - | - |  | - | 220 |  |
| Stage 2 | - |  |  |  | 249 |  |
| Platoon blocked, \% | - | - |  |  |  |  |
| Mov Cap-1 Maneuver | - |  | 465 |  | $\sim 18$ | 165 |
| Mov Cap-2 Maneuver |  | - |  |  | $\sim 18$ |  |
| Stage 1 |  | - |  |  | 220 |  |
| Stage 2 | - | - | - |  | 200 |  |


|  | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| Approach | 1.1 | $\$ 1477.1$ |  |
| HCM Control Delay, s | 0 | 1 | F |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 36 | - | -465 | - |  |
| HCM Lane V/C Ratio | 3.774 | - | -0.199 | - |  |
| HCM Control Delay (s) | $\$ 1477.1$ | - | -14.7 | - |  |
| HCM Lane LOS | F | - | - | B | - |
| HCM 95th \%tile Q(veh) | 15.7 | - | - | 0.7 | - |

[^3]| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay，s／veh | 0.2 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 个中 | 个． | $\mathbf{F}$ |  | $\mathbf{7}$ |
| Traffic Vol，veh／h | 0 | 1387 | 1097 | 84 | 0 | 34 |
| Future Vol，veh／h | 0 | 1387 | 1097 | 84 | 0 | 34 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | 0 | - | 0 |
| Veh in Median Storage，\＃ | - | 0 | 0 | - | 0 | - |
| Grade，\％ | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 1508 | 1192 | 91 | 0 | 37 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh | 26 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | 「 |  |  | 「゙ |  | 中 ${ }^{\text {a }}$ |  |  | 中 ${ }^{\text {a }}$ |  |
| Traffic Vol，veh／h | 0 | 0 | 109 | 0 | 0 | 475 | 0 | 1034 | 120 | 0 | 912 | 48 |
| Future Vol，veh／h | 0 | 0 | 109 | 0 | 0 | 475 | 0 | 1034 | 120 | 0 | 912 | 48 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | － | － | None | － | － | None | － | － | None | － | － | None |
| Storage Length | － | － | 0 | － | － | 0 | － | － | － | － | － | － |
| Veh in Median Storage，\＃ | \＃ | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 118 | 0 | 0 | 516 | 0 | 1124 | 130 | 0 | 991 | 52 |



Platoon blocked，\％
Mov Cap－1 Maneuver－－ 499 －$\sim 426$

Mov Cap－2 Maneuver
Stage 1
Stage 2

| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay，s | 14.4 | 144.1 | 0 | 0 |
| HCM LOS | B | F |  |  |


| Minor Lane／Major Mvmt | NBT | NBR EBLn1WBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity（veh／h） | - | - | 499 | 426 | - |

## Notes

$\sim$ ：Volume exceeds capacity $\$$ ：Delay exceeds 300s $\quad+$ ：Computation Not Defined $\quad$ ：All major volume in platoon

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.4 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations |  | $\mathbf{7}$ |  | 体 | 怍 |  |
| Traffic Vol, veh/h | 0 | 170 | 90 | 1419 | 790 | 55 |
| Future Vol, veh/h | 0 | 170 | 90 | 1419 | 790 | 55 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | 0 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 185 | 98 | 1542 | 859 | 60 |



| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 14.9 | 0.6 | 0 |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |
| :--- | ---: | ---: | ---: | :---: |
| Capacity (veh/h) | 738 | - | 548 | - |

## Operational Data

Main Geometry (ft)

## Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> ? |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 0 | 12.00 | 1 | 14.00 | 1 | 55.00 | 50.00 | 20.00 |
| 2 | West Leg | 90 | 0 | 24.00 | 2 | 25.70 | 2 | 70.00 | 40.00 | 20.00 |
| 3 | South Leg | 160 | 0 | 12.10 | 1 | 24.00 | 2 | 130.00 | 60.00 | 20.00 |
| 4 | East Leg | 265 | 0 | 22.30 | 2 | 24.00 | 2 | 180.00 | 60.00 | 20.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> D | Circulating <br> Width <br> C | Circulating <br> Lanes <br> $\mathbf{n c}$ | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 165.00 | 30.00 | 2 | 24.70 | 2 | 23.30 | 2 |
| 2 | West Leg | 140.00 | 20.00 | 1 | 25.10 | 2 | 24.00 | 2 |
| 3 | South Leg | 165.00 | 30.00 | 2 | 25.00 | 1 | 12.20 | 1 |
| 4 | East Leg | 140.00 | 30.00 | 2 | 24.00 | 2 | 19.40 | 2 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity |  | Entry Calibration |  | Approach Road |  |  | Exit Road |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity + or - | XWalk Factor | Intercept + or - | Slope Factor | V $(\mathrm{ft})$ | Default Capacity | Calib Capacity | $(\mathrm{ft})$ | Default Capacity | Calib Capacity |
| 1 | North Leg | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 23.30 | 3480 | 0 |
| 2 | West Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 3 | South Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 1807 | 0 | 12.20 | 1822 | 0 |
| 4 | East Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3331 | 0 | 19.40 | 2897 | 0 |

## Bypass Geometry

Bypass Approach Geometry (ft)

| Leg | Leg Names | Bypass <br> Type | Bypass <br> Flows | V | nv | Vb | nvb | Vt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | Yield | 470 | 12 | 1 | 12 | 1 | 24 |

Bypass Entry and Exit Geometry (ft)

| Leg | Leg Names | Eb | neb | Lb | Lt | Rb | Phib | Leg | Leg Names | Exit Lanes <br> nex | Nmx |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | North Leg | 12 | 1 | 20 | 130 | 65.00024 <br> 752 | 30 | 2 | West Leg | 2 | 2 |

Bypass Entry Capacity Modifiers and Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity <br> Capacity <br> + or - |  | Cross Walk <br> Factor | Intercept <br> + or - |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 1.000 | 0 | Slope <br> Factor |

## Traffic Flow Data (veh/hr)

2040 AM Peak Peak Hour Flows

| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks <br> $\%$ | Flow Modifiers <br> Flow <br> Factor | Peak Hour <br> Factor |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 260 | 270 | 0 | 470 | 2.0 | 1.00 | 0.9 |
| 2 | West Leg | 0 | 717 | 642 | 75 | 0 | 2.0 | 1.00 | 0.9 |
| 3 | South Leg | 0 | 81 | 330 | 260 | 0 | 2.0 | 1.00 | 0.9 |
| 4 | East Leg | 0 | 170 | 294 | 155 | 0 | 2.0 | 1.00 | 0.9 |

## Operational Results

## 2040 AM Peak - 60 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit <br> Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | North Leg | Yield | 530 | 470 | 545 | 545 | 1195 | 980 | 895 | 0.5508 | 0.5356 |
| 2 | West Leg | None | 1434 |  | 700 |  | 844 | 1544 |  | 1.0156 |  |
| 3 | South Leg | None | 671 |  | 1608 |  | 514 | 880 |  | 0.8053 |  |
| 4 | East Leg | None | 619 |  | 1121 |  | 1156 | 1358 |  | 0.4631 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | North Leg | Yield | 7.56 | 8.35 | 7.93 | 3.24 | 3.16 | A | A | A |
| 2 | West Leg | None | 42.99 |  | 42.99 | 52.03 |  | E |  | E |
| 3 | South Leg | None | 24.81 |  | 24.81 | 14.13 |  | C |  | C |
| 4 | East Leg | None | 6.40 |  | 6.40 | 3.21 |  | A |  | A |

## 2040 AM Peak - 15 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit <br> Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | North Leg | Yield | 558 | 495 | 572 | 572 | 1234 | 969 | 885 | 0.5850 | 0.5691 |
| 2 | West Leg | None | 1509 |  | 736 |  | 887 | 1507 |  | 1.0923 |  |
| 3 | South Leg | None | 706 |  | 1654 |  | 539 | 850 |  | 0.8752 |  |
| 4 | East Leg | None | 652 |  | 1155 |  | 1195 | 1333 |  | 0.4958 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | North Leg | Yield | 7.80 | 8.62 | 8.19 | 3.24 | 3.16 | A | A | A |
| 2 | West Leg | None | 48.55 |  | 48.55 | 52.03 |  | E |  | E |
| 3 | South Leg | None | 26.97 |  | 26.97 | 14.13 |  | D |  | D |
| 4 | East Leg | None | 6.59 |  | 6.59 | 3.21 |  | A |  | A |

## Global Results

## Performance and Accidents

2040 AM Peak Global Performance

| Parameter | Units | Entries | Bypasses | Total |
| :--- | :---: | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 3254 | 470 | 3724 |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 4762 | 895 | 5657 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 26.51 | 8.35 | 24.22 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | C | A | C |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | D | A | C |
| Total Delay | veh.hrs | 23.96 | 1.09 | 25.05 |






Platoon blocked, \%

| Mov Cap-1 Maneuver | - | - | 485 | - | - | 411 | - | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - | - | - | - | - | - | - |

Stage 2

| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, s | 12.6 | 15.6 | 0 | 0 |
| HCM LOS | B | C |  |  |


| Minor Lane/Major Mvmt | NBT | NBR EBLn1WBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | - | -485 | 411 | - | - |
| HCM Lane V/C Ratio | - | -0.022 | 0.172 | - | - |
| HCM Control Delay (s) | - | -12.6 | 15.6 | - | - |
| HCM Lane LOS | - | - | B | C | - |
| HCM 95th \%tile Q(veh) | - | - | 0.1 | 0.6 | - |
| H |  | - |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |



| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 12.6 | 0.2 | 0 |
| HCM LOS | B |  |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |
| :--- | ---: | ---: | ---: | :---: |
| Capacity (veh/h) | 640 | -485 | - | - |
| HCM Lane V/C Ratio | 0.034 | -0.022 | - | - |
| HCM Control Delay (s) | 10.8 | -12.6 | - | - |
| HCM Lane LOS | B | - | $B$ | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | 0.1 | - |
| (ven |  |  |  |  |

## Operational Data

## Main Geometry (ft)

## Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> ? |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 0 | 12.00 | 1 | 14.00 | 1 | 55.00 | 50.00 | 20.00 |
| 2 | West Leg | 90 | 0 | 24.00 | 2 | 25.70 | 2 | 70.00 | 40.00 | 20.00 |
| 3 | South Leg | 160 | 0 | 12.10 | 1 | 24.00 | 2 | 130.00 | 60.00 | 20.00 |
| 4 | East Leg | 265 | 0 | 22.30 | 2 | 24.00 | 2 | 180.00 | 60.00 | 20.00 |

## Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> D | Circulating <br> Width <br> C | Circulating <br> Lanes <br> $\mathbf{n c}$ | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 165.00 | 30.00 | 2 | 24.70 | 2 | 23.30 | 2 |
| 2 | West Leg | 140.00 | 20.00 | 1 | 25.10 | 2 | 24.00 | 2 |
| 3 | South Leg | 165.00 | 30.00 | 2 | 25.00 | 1 | 12.20 | 1 |
| 4 | East Leg | 140.00 | 30.00 | 2 | 24.00 | 2 | 19.40 | 2 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity |  | Entry Calibration |  | Approach Road |  |  | Exit Road |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity + or - | XWalk Factor | Intercept + or - | Slope Factor | V $(\mathrm{ft})$ | Default Capacity | Calib Capacity | $(\mathrm{ft})$ | Default Capacity | Calib Capacity |
| 1 | North Leg | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 23.30 | 3480 | 0 |
| 2 | West Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 3 | South Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 1807 | 0 | 12.20 | 1822 | 0 |
| 4 | East Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3331 | 0 | 19.40 | 2897 | 0 |

## Bypass Geometry

Bypass Approach Geometry (ft)

| Leg | Leg Names | Bypass <br> Type | Bypass <br> Flows | V | nv | Vb | nvb | Vt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | Yield | 743 | 12 | 1 | 12 | 1 | 24 |

Bypass Entry and Exit Geometry (ft)

| Leg | Leg Names | Eb | neb | Lb | Lt | Rb | Phib | Leg | Leg Names | Exit Lanes <br> nex | Nmx |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | North Leg | 12 | 1 | 20 | 130 | 65.00025 <br> 376 | 30 | 2 | West Leg | 2 | 2 |

Bypass Entry Capacity Modifiers and Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity <br> Capacity <br> + or - |  | Cross Walk <br> Factor | Intercept <br> + or - |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 1.000 | 0 | Slope <br> Factor |

## Traffic Flow Data (veh/hr)

2040 PM Peak Peak Hour Flows

| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks <br> $\%$ | Flow Modifiers <br> Flow <br> Factor | Peak Hour <br> Factor |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 195 | 280 | 0 | 743 | 2.0 | 1.00 | 0.9 |
| 2 | West Leg | 0 | 457 | 309 | 33 | 0 | 2.0 | 1.00 | 0.9 |
| 3 | South Leg | 0 | 86 | 310 | 290 | 0 | 2.0 | 1.00 | 0.9 |
| 4 | East Leg | 0 | 290 | 536 | 250 | 0 | 2.0 | 1.00 | 0.9 |

## Operational Results

## 2040 PM Peak - 60 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | North Leg | Yield | 475 | 743 | 912 | 912 | 1017 | 844 | 765 | 0.5755 | 1.1275 |
| 2 | West Leg | None | 799 |  | 765 |  | 1348 | 1476 |  | 0.5528 |  |
| 3 | South Leg | None | 686 |  | 961 |  | 603 | 1311 |  | 0.5353 |  |
| 4 | East Leg | None | 1076 |  | 853 |  | 794 | 1557 |  | 0.7065 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | North Leg | Yield | 9.19 | 78.61 | 51.53 | 3.61 | 45.84 | A | F | F |
| 2 | West Leg | None | 8.76 |  | 8.76 | 5.70 |  | A |  | A |
| 3 | South Leg | None | 9.43 |  | 9.43 | 5.23 |  | A |  | A |
| 4 | East Leg | None | 9.45 |  | 9.45 | 8.45 |  | A |  | A |

## 2040 PM Peak - 15 minutes

Flows and Capacity

| Leg | Leg Names | Bypass Type | Flows (veh/hr) |  |  |  |  | Capacity (veh/hr) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Arrival Flow |  | Opposing Flow |  | Exit <br> Flow | Capacity |  | Average VCR |  |
|  |  |  | Entry | Bypass | Entry | Bypass |  | Entry | Bypass | Entry | Bypass |
| 1 | North Leg | Yield | 500 | 782 | 957 | 957 | 1068 | 827 | 749 | 0.6171 | 1.1928 |
| 2 | West Leg | None | 841 |  | 803 |  | 1386 | 1436 |  | 0.5971 |  |
| 3 | South Leg | None | 722 |  | 1009 |  | 633 | 1278 |  | 0.5767 |  |
| 4 | East Leg | None | 1133 |  | 896 |  | 834 | 1525 |  | 0.7584 |  |

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass Type | Average Delay (sec) |  |  | 95\% Queue (veh) |  | Level of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | North Leg | Yield | 9.63 | 83.76 | 54.85 | 3.61 | 45.84 | A | F | F |
| 2 | West Leg | None | 9.25 |  | 9.25 | 5.70 |  | A |  | A |
| 3 | South Leg | None | 9.87 |  | 9.87 | 5.23 |  | A |  | A |
| 4 | East Leg | None | 10.28 |  | 10.28 | 8.45 |  | B |  | B |

## Global Results

## Performance and Accidents

2040 PM Peak Global Performance

| Parameter | Units | Entries | Bypasses | Total |
| :--- | :---: | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 3036 | 743 | 3779 |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 5188 | 765 | 5953 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 9.22 | 78.61 | 22.87 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | A | E | C |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | A | F | C |
| Total Delay | veh.hrs | 7.78 | 16.22 | 24.00 |



| Major/Minor M | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 815 | 0 | 1684 | 408 |
| Stage 1 | - | - | - | - | 804 | - |
| Stage 2 | - | - | - | - | 880 | - |
| Critical Hdwy | - | - | 4.14 | - | 6.84 | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.84 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.84 | - |
| Follow-up Hdwy | - | - | 2.22 | - | 3.52 | 3.32 |
| Pot Cap-1 Maneuver | - | - | 808 | - | 85 | 593 |
| Stage 1 | - | - | - | - | 401 | - |
| Stage 2 | - | - | - | - | 366 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 808 | - | 75 | 593 |
| Mov Cap-2 Maneuver | - | - | - | - | 75 | - |
| Stage 1 | - | - | - | - | 401 | - |
| Stage 2 | - | - | - | - | 324 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.6 |  | 114.8 |  |
| HCM LOS |  |  |  |  | F |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) |  | 147 | - | - | 808 | - |
| HCM Lane V/C Ratio |  | 0.924 | - | - | 0.114 | - |
| HCM Control Delay (s) |  | 114.8 | - | - | 10 | - |
| HCM Lane LOS |  | F | - | - | B | - |
| HCM 95th \%tile Q(veh) |  | 6.5 | - | - | 0.4 | - |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh | 16.9 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | 「゙ |  |  | 「゙ |  | 中 ${ }^{\text {a }}$ |  |  | 中 ${ }^{\text {a }}$ |  |
| Traffic Vol，veh／h | 0 | 0 | 20 | 0 | 0 | 475 | 0 | 895 | 125 | 0 | 1200 | 5 |
| Future Vol，veh／h | 0 | 0 | 20 | 0 | 0 | 475 | 0 | 895 | 125 | 0 | 1200 | 5 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | － | － | None | － | － | None | － | － | None | － | － | None |
| Storage Length | － | － | 0 | － | － | 0 | － | － | － | － | － | － |
| Veh in Median Storage，\＃ | \＃ | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 22 | 0 | 0 | 516 | 0 | 973 | 136 | 0 | 1304 | 5 |



Platoon blocked，\％
Mov Cap－1 Maneuver－－ 409 －-475

Mov Cap－2 Maneuver
Stage 1
Stage 2

| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay，s | 14.3 | 96.1 | 0 | 0 |

HCM LOS
B F

| Minor Lane／Major Mvmt | NBT | NBR EBLn1WBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity（veh／h） | - | -409 | 475 | - | - |
| HCM Lane V／C Ratio | - | -0.053 | 1.087 | - | - |
| HCM Control Delay（s） | - | -14.3 | 96.1 | - | - |
| HCM Lane LOS | - | - | B | F | - |
| HCM 95th \％tile Q（veh） | - | - | 0.2 | 16.7 | - |

Notes
$\sim$ ：Volume exceeds capacity $\$$ ：Delay exceeds 300s $\quad+$ ：Computation Not Defined $\quad$ ：All major volume in platoon

Synchro 10 Report



| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 18.5 | 0.8 | 0 |
| HCM LOS | C |  |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |
| :--- | ---: | ---: | ---: | :---: |
| Capacity (veh/h) | 585 | - | 449 | - |
| HCM Lane V/C Ratio | 0.167 | -0.412 | - | - |
| HCM Control Delay (s) | 12.4 | - | 18.5 | - |
| HCM Lane LOS | B | - | C | - |
| HCM 95th \%tile Q(veh) | 0.6 | - | 2 | - |

## Scheme Summary

## Control Data

Control Data and Model Parameters

| West End | 2040 PHF Flow Profile (veh) |
| :--- | :--- |
| 2040 Total Traffic | 7.5 min Time Slice |
| Rodel-Win1 | Queuing Delays (sec) |
| Right Hand Drive | Daylight conditions |
| AM Peak Hour | Peak $60 / 15$ min Results |
| Full Geometry | Output flows: Vehicles |
| English Units (ft) | $50 \%$ Confidence Level |

## Available Data

| Entry Capacity Calibrated | No |
| :--- | :---: |
| Entry Capacity Modified | No |
| Crosswalks | No |
| Flows Factored | No |
| Approach/Exit Road Capacity Calibrated | No |
| Accidents | No |
| Accident Costs | No |
| Bypass Model | Yes |
| Bypass Calibration | No |
| Global Results | Yes |

## Operational Data

## Main Geometry (ft)

## Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> $\boldsymbol{\Phi}$ |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 0 | 12.00 | 1 | 14.00 | 1 | 55.00 | 50.00 | 20.00 |
| 2 | West Leg | 90 | 0 | 24.00 | 2 | 25.70 | 2 | 70.00 | 40.00 | 20.00 |
| 3 | South Leg | 160 | 0 | 12.10 | 1 | 24.00 | 2 | 130.00 | 60.00 | 20.00 |
| 4 | East Leg | 265 | 0 | 22.30 | 2 | 24.00 | 2 | 180.00 | 60.00 | 20.00 |

## Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> $\mathbf{D}$ | Circulating <br> Width <br> $\mathbf{C}$ | Circulating <br> Lanes <br> $\mathbf{n c}$ | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 165.00 | 30.00 | 2 | 24.70 | 2 | 23.30 | 2 |
| 2 | West Leg | 140.00 | 20.00 | 1 | 25.10 | 2 | 24.00 | 2 |
| 3 | South Leg | 165.00 | 30.00 | 2 | 25.00 | 1 | 12.20 | 1 |
| 4 | East Leg | 140.00 | 30.00 | 2 | 24.00 | 2 | 19.40 | 2 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity |  | Entry Calibration |  | Approach Road |  |  | Exit Road |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity + or - | XWalk Factor | Intercept + or - | Slope <br> Factor | $\begin{gathered} \mathbf{V} \\ (\mathrm{ft}) \end{gathered}$ | Default Capacity | Calib Capacity | $\begin{gathered} \mathbf{V} \\ (\mathrm{ft}) \end{gathered}$ | Default Capacity | Calib Capacity |
| 1 | North Leg | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 23.30 | 3480 | 0 |
| 2 | West Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 3 | South Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 1807 | 0 | 12.20 | 1822 | 0 |
| 4 | East Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3331 | 0 | 19.40 | 2897 | 0 |

## Bypass Geometry

Bypass Approach Geometry (ft)

| Leg | Leg Names | Bypass <br> Type | Bypass <br> Flows | $\mathbf{V}$ | nv | Vb | nvb | Vt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | Yield | 470 | 12 | 1 | 12 | 1 | 24 |

Bypass Entry and Exit Geometry (ft)

| Leg | Leg Names | Eb | neb | Lb | Lt | Rb | Phib | Leg | Leg Names |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 12 | 1 | 20 | 130 | 65.00021 <br> 216 | 30 | 2 | West Leg |
| nex |  | 2 | 2 |  |  |  |  |  |  |

## Bypass Entry Capacity Modifiers and Calibration (veh/hr)

| Leg | Leg Names | Capacity <br> + or - | Entry Capacity <br> Cross Walk <br> Factor | Intercept <br> + or - | Calibration <br> Factor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 1.000 | 0 | 1.000 |

## Traffic Flow Data (veh/hr)

## 2040 AM Peak Peak Hour Flows

| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks <br> $\%$ | Flow Modifiers <br> Flow <br> Factor | Peak Hour <br> Factor |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 49 | 294 | 286 | 0 | 470 | 2.0 | 1.00 | 0.9 |
| 2 | West Leg | 21 | 712 | 642 | 75 | 0 | 2.0 | 1.00 | 0.9 |
| 3 | South Leg | 0 | 96 | 326 | 260 | 0 | 2.0 | 1.00 | 0.9 |
| 4 | East Leg | 0 | 170 | 312 | 155 | 0 | 2.0 | 1.00 | 0.9 |

## Operational Results

## 2040 AM Peak - 60 minutes

## Delays, Queues and Level of Service

| Leg | Leg Names | Bypass | Average Delay (sec) |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  | Entry | Bypass |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Leg | Entry | Bypass | Entry | Bypass | Leg |  |  |  |
| 1 | North Leg | Yield | 10.08 | 8.73 | 9.50 | 5.20 | 3.32 | B | A | A |
| 2 | West Leg | None | 91.63 |  | 91.63 | 105.91 |  | F | F |  |
| 3 | South Leg | None | 31.28 |  | 31.28 | 16.55 | D | D |  |  |
| 4 | East Leg | None | 6.86 |  | 6.86 | 3.49 | A | A |  |  |

## 2040 AM Peak - 15 minutes

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass | Average Delay (sec) |  |  | $95 \%$ Queue (veh) |  | Level of Service <br> Type |  | Entry |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |  |  |
| 1 | North Leg | Yield | 10.62 | 9.03 | 9.94 | 5.20 | 3.32 | B | A | A |
| 2 | West Leg | None | 92.48 |  | 92.48 | 105.91 |  | F | F |  |
| 3 | South Leg | None | 32.82 |  | 32.82 | 16.55 | D | D |  |  |
| 4 | East Leg | None | 7.04 |  | 7.04 | 3.49 | A | A |  |  |

## Global Results

## Performance and Accidents

## 2040 AM Peak Global Performance

| Parameter | Units | Entries | Bypasses | Total |
| :--- | :---: | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 3398 | 470 | 3868 |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 4552 | 876 | 5428 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 48.53 | 8.73 | 43.69 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | D | A | D |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | E | A | E |
| Total Delay | veh.hrs | 45.81 | 1.14 | 46.95 |

2: Commercial Access \& SH 6

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.8 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 个4 | $\mathbf{r}$ | 1 | $\mathbf{4}$ | ric |  |
| Traffic Vol, veh/h | 1431 | 20 | 25 | 849 | 10 | 20 |
| Future Vol, veh/h | 1431 | 20 | 25 | 849 | 10 | 20 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 140 | 60 | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1555 | 22 | 27 | 923 | 11 | 22 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay，s／veh | 0.2 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 个中 | 个． | $\mathbf{F}$ |  | $\mathbf{7}$ |
| Traffic Vol，veh／h | 0 | 1451 | 835 | 64 | 0 | 39 |
| Future Vol，veh／h | 0 | 1451 | 835 | 64 | 0 | 39 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | 0 | - | 0 |
| Veh in Median Storage，\＃ | - | 0 | 0 | - | 0 | - |
| Grade，\％ | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 1577 | 908 | 70 | 0 | 42 |





Platoon blocked, \%

| Mov Cap-1 Maneuver | - | - | 477 | - | - | 397 | - | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - | - | - | - | - | - | - |

Stage 2

| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | :---: | :---: |
| HCM Control Delay, S | 15.3 | 16 | 0 | 0 |
| HCM LOS | C | C |  |  |


| Minor Lane/Major Mvmt | NBT | NBR EBLn1WBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | - | -477 | 397 | - | - |
| HCM Lane V/C Ratio | - | -0.271 | 0.178 | - | - |
| HCM Control Delay (s) | - | - | 15.3 | 16 | - |
| HCM Lane LOS | - | - | $C$ | C | - |
| HCM 95th \%tile Q(veh) | - | - | 1.1 | 0.6 | - |
| H |  | - |  |  |  |

5: Edwards Access Road \& Commercial Access

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Minor2 |  | Major1 | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 552 | 1103 | 0 | - | 0 |  |
| Stage 1 | - | - | - | - | - | - |  |
| Stage 2 | - |  | - | - | - | - |  |
| Critical Hdwy | - | 6.94 | 4.14 | - | - | - |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |  |
| Follow-up Hdwy | - | 3.32 | 2.22 | - | - | - |  |
| Pot Cap-1 Maneuver | 0 | 477 | 629 | - | - | - |  |
| Stage 1 | 0 | - | - | - | - | - |  |
| Stage 2 | 0 | - | - | - | - | - |  |
| Platoon blocked, \% |  |  |  | - | - | - |  |
| Mov Cap-1 Maneuver | - | 477 | 629 | - | - | - |  |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |  |
| Stage 1 | - | - | - | - | - | - |  |
| Stage 2 | - | - | - | - | - | - |  |



## Scheme Summary

## Control Data

Control Data and Model Parameters

| West End | 2040 PHF Flow Profile (veh) |
| :--- | :--- |
| 2040 Total Traffic | 7.5 min Time Slice |
| Rodel-Win1 | Queuing Delays (sec) |
| Right Hand Drive | Daylight conditions |
| PM Peak Hour | Peak $60 / 15$ min Results |
| Full Geometry | Output flows: Vehicles |
| English Units (ft) | $50 \%$ Confidence Level |

## Available Data

| Entry Capacity Calibrated | No |
| :--- | :---: |
| Entry Capacity Modified | No |
| Crosswalks | No |
| Flows Factored | No |
| Approach/Exit Road Capacity Calibrated | No |
| Accidents | No |
| Accident Costs | No |
| Bypass Model | Yes |
| Bypass Calibration | No |
| Global Results | Yes |

## Operational Data

## Main Geometry (ft)

## Approach and Entry Geometry

| Leg | Leg Names | Approach <br> Bearing <br> (deg) | Grade <br> Separation <br> $\mathbf{G}$ | Half Width <br> $\mathbf{V}$ | Approach <br> Lanes <br> $\mathbf{n}$ | Entry <br> Width <br> $\mathbf{E}$ | Entry <br> Lanes <br> $\mathbf{n}$ | Flare <br> Length <br> $\mathbf{L}^{\prime}$ | Entry <br> Radius <br> $\mathbf{R}$ | Entry <br> Angle <br> $\boldsymbol{\Phi}$ |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 0 | 12.00 | 1 | 14.00 | 1 | 55.00 | 50.00 | 20.00 |
| 2 | West Leg | 90 | 0 | 24.00 | 2 | 25.70 | 2 | 70.00 | 40.00 | 20.00 |
| 3 | South Leg | 160 | 0 | 12.10 | 1 | 24.00 | 2 | 130.00 | 60.00 | 20.00 |
| 4 | East Leg | 265 | 0 | 22.30 | 2 | 24.00 | 2 | 180.00 | 60.00 | 20.00 |

## Circulating and Exit Geometry

| Leg | Leg Names | Inscribed <br> Diameter <br> $\mathbf{D}$ | Circulating <br> Width <br> $\mathbf{C}$ | Circulating <br> Lanes <br> $\mathbf{n c}$ | Exit <br> Width <br> Ex | Exit <br> Lanes <br> nex | Exit <br> Half Width <br> Vx | Exit Half <br> Width Lanes <br> nvx |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 165.00 | 30.00 | 2 | 24.70 | 2 | 23.30 | 2 |
| 2 | West Leg | 140.00 | 20.00 | 1 | 25.10 | 2 | 24.00 | 2 |
| 3 | South Leg | 165.00 | 30.00 | 2 | 25.00 | 1 | 12.20 | 1 |
| 4 | East Leg | 140.00 | 30.00 | 2 | 24.00 | 2 | 19.40 | 2 |

Capacity Modifiers and Capacity Calibration (veh/hr)

| Leg | Leg Names | Entry Capacity |  | Entry Calibration |  | Approach Road |  |  | Exit Road |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity + or - | XWalk Factor | Intercept + or - | Slope <br> Factor | $\begin{gathered} \mathbf{V} \\ (\mathrm{ft}) \end{gathered}$ | Default Capacity | Calib Capacity | $\begin{gathered} \mathbf{V} \\ (\mathrm{ft}) \end{gathered}$ | Default Capacity | Calib Capacity |
| 1 | North Leg | 0 | 1.000 | 0 | 1.000 | 24.00 | 3584 | 0 | 23.30 | 3480 | 0 |
| 2 | West Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3584 | 0 | 24.00 | 3584 | 0 |
| 3 | South Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 1807 | 0 | 12.20 | 1822 | 0 |
| 4 | East Leg | 0 | 1.000 | 0 | 1.000 | 20.00 | 3331 | 0 | 19.40 | 2897 | 0 |

## Bypass Geometry

Bypass Approach Geometry (ft)

| Leg | Leg Names | Bypass <br> Type | Bypass <br> Flows | $\mathbf{V}$ | nv | Vb | nvb | Vt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | Yield | 743 | 12 | 1 | 12 | 1 | 24 |

Bypass Entry and Exit Geometry (ft)

| Leg | Leg Names | Entry Geometry |  |  |  |  |  | Leg | Leg Names | Exit Lanes |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Eb | neb | Lb | Lt | Rb | Phib |  |  | nex | Nmx |
| 1 | North Leg | 12 | 1 | 20 | 130 | $\begin{gathered} 65.00022 \\ 256 \end{gathered}$ | 30 | 2 | West Leg | 2 | 2 |

## Bypass Entry Capacity Modifiers and Calibration (veh/hr)

| Leg | Leg Names | Capacity <br> + or - | Entry Capacity <br> Cross Walk <br> Factor | Intercept <br> + or - | Calibration <br> Flope |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 0 | 1.000 | 0 | 1.000 |

## Traffic Flow Data (veh/hr)

## 2040 PM Peak Peak Hour Flows

| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks <br> $\%$ | Flow Modifiers <br> Flow <br> Factor | Peak Hour <br> Factor |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | North Leg | 40 | 223 | 293 | 0 | 743 | 2.0 | 1.00 | 0.9 |
| 2 | West Leg | 30 | 454 | 309 | 33 | 0 | 2.0 | 1.00 | 0.9 |
| 3 | South Leg | 0 | 103 | 307 | 290 | 0 | 2.0 | 1.00 | 0.9 |
| 4 | East Leg | 0 | 290 | 565 | 250 | 0 | 2.0 | 1.00 | 0.9 |

2040 PM Peak
Project: West End
50\% Confidence Level
Daylight conditions

Scheme: 2040 Total Traffic
Rodel-Win1 - Full Geometry

## Operational Results

## 2040 PM Peak - 60 minutes

## Delays, Queues and Level of Service

| Leg | Leg Names | Bypass | Average Delay (sec) |  | $95 \%$ Queue (veh) |  | Level of Service |  |  |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Type | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | North Leg | Yield | 12.76 | 109.81 | 68.27 | 6.01 | 64.09 | B | F | F |
| 2 | West Leg | None | 10.17 |  | 10.17 | 6.95 |  | B | B |  |
| 3 | South Leg | None | 10.55 |  | 10.55 | 6.03 | B | B |  |  |
| 4 | East Leg | None | 11.33 |  | 11.33 | 10.62 | B | B |  |  |

2040 PM Peak
Project: West End
50\% Confidence Level
Daylight conditions

Scheme: 2040 Total Traffic
Rodel-Win1 - Full Geometry

## 2040 PM Peak - 15 minutes

Delays, Queues and Level of Service

| Leg | Leg Names | Bypass | Average Delay (sec) |  |  | $95 \%$ Queue (veh) |  | Level of Service |  |  |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Type | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | North Leg | Yield | 13.73 | 116.83 | 72.70 | 6.01 | 62.35 | B | F | F |
| 2 | West Leg | None | 10.91 |  | 10.91 | 6.95 |  | B | B |  |
| 3 | South Leg | None | 11.15 |  | 11.15 | 6.03 |  | B |  |  |
| 4 | East Leg | None | 12.59 |  | 12.59 | 10.62 | B | B |  |  |

## Global Results

## Performance and Accidents

## 2040 PM Peak Global Performance

| Parameter | Units | Entries | Bypasses | Total |
| :--- | :---: | :---: | :---: | :---: |
| Arrive Flows | $\mathrm{veh} / \mathrm{hr}$ | 3187 | 743 | 3930 |
| Capacity | $\mathrm{veh} / \mathrm{hr}$ | 4953 | 739 | 5692 |
| Average Delay | $\mathrm{sec} / \mathrm{veh}$ | 11.11 | 109.81 | 29.77 |
| L.O.S. (Signal) | $\mathrm{A}-\mathrm{F}$ | B | F | C |
| L.O.S. (Unsig) | $\mathrm{A}-\mathrm{F}$ | B | F | D |
| Total Delay | veh.hrs | 9.83 | 22.66 | 32.50 |



| Major/Minor M | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 845 | 0 | 1717 | 412 |
| Stage 1 | - | - | - | - | 823 | - |
| Stage 2 | - | - | - | - | 894 | - |
| Critical Hdwy | - | - | 4.14 | - | 6.84 | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.84 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.84 | - |
| Follow-up Hdwy | - | - | 2.22 | - | 3.52 | 3.32 |
| Pot Cap-1 Maneuver | - | - | 787 | - | 81 | 589 |
| Stage 1 | - | - | - | - | 392 | - |
| Stage 2 | - | - | - | - | 360 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 787 | - | 72 | 589 |
| Mov Cap-2 Maneuver | - | - | - | - | 72 | - |
| Stage 1 | - | - | - | - | 392 | - |
| Stage 2 | - | - | - | - | 318 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.6 |  | 125.6 |  |
| HCM LOS |  |  |  |  | F |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) |  | 142 | - | - | 787 | - |
| HCM Lane V/C Ratio |  | 0.957 | - | - | 0.117 | - |
| HCM Control Delay (s) |  | 125.6 | - | - | 10.2 | - |
| HCM Lane LOS |  | F | - | - | B | - |
| HCM 95th \%tile Q(veh) |  | 6.8 | - | - | 0.4 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay，s／veh | 0.2 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 个4 | 个中 | $\mathbf{F}$ |  | $\mathbf{7}$ |
| Traffic Vol，veh／h | 0 | 827 | 1357 | 84 | 0 | 34 |
| Future Vol，veh／h | 0 | 827 | 1357 | 84 | 0 | 34 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | 0 | - | 0 |
| Veh in Median Storage，\＃ | - | 0 | 0 | - | 0 | - |
| Grade，\％ | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 899 | 1475 | 91 | 0 | 37 |



| Intersection |  | 18 |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |



Platoon blocked, \%
Mov Cap-1 Maneuver - - 397 - $\sim 465$

## Mov Cap-2 Maneuver

Stage 1
Stage 2

| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, s | 18.4 | 104.5 | 0 | 0 |
| HCM LOS | C | F |  |  |


| Minor Lane/Major Mvmt | NBT | NBR EBLn1WBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | - | - | 397 | 465 | - |

## Notes

$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.6 |  |  |  |  |  |
| Movement E | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations |  | F' | ${ }^{7}$ | 44 | 中 ${ }^{\text {F }}$ |  |
| Traffic Vol, veh/h | 0 | 170 | 90 | 1314 | 1070 | 55 |
| Future Vol, veh/h | 0 | 170 | 90 | 1314 | 1070 | 55 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Stop | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | 0 | - | - | - |
| Veh in Median Storage, \# | \# 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 185 | 98 | 1428 | 1163 | 60 |



| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 19.2 | 0.8 | 0 |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 566 | - | 436 | - |


[^0]:    ${ }^{1}$ A future deceleration lane could be required if/when Edwards Plaza redevelops.

[^1]:    File Name : EDWAUS6
    Site Code : 00000014
    Start Date : 3/4/2020
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[^2]:    Notes
    $\sim$ : Volume exceeds capacity $\quad \$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

[^3]:    Notes
    $\sim$ : Volume exceeds capacity $\$$ : Delay exceeds $300 \mathrm{~s} \quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

